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Theoretical study of the mechanism of 2,5-diketopiperazine formation during pyrolysis of proline

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Theoretical study of the mechanism of 2,5diketopiperazine formation during pyrolysis of proline

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ABSTRACT

The mechanism of formation of 2,5-diketopiperazine upon pyrolysis of proline at 300°C was theoretically studied by means of DFT calculations (wB97XD/6-311g(d,p)). All transition states and minimum energy structures involved were optimized, and thermodynamic parameters were theoretically estimated. The reaction occurs through a mechanism of four steps where the second one, which consists in a dehydration process, contains the highest activation enthalpy. The latter step was analyzed by using the reaction force formalism, and an analysis of geometrical parameters, charge distributions and bond orders. The results show that the first intermediate (INT1) and its subsequent transition state (TS2) are the most important rate-controlling states. The energetic barrier is formed by a 75% of geometrical rearrangements while the proton transfer needed to form water and achieve the dehydration represents the remaining 25%. INT1 appears to be a very stable intermediate due to the high dominancy of geometrical rearrangements for both, the forward and the reverse reaction. Changes of less than ± 0.1 in the charges of atoms demonstrate that charge transfer is not an important factor for the analyzed reaction step. Finally, from the bond order analysis, it is determined that TS2 is an early transition state, and that the process is asynchronous.

1. INTRODUCTION

The pyrolysis of organic compounds is an important process in which a substrate thermally decomposes upon exposure to temperatures above 200°C. It involves changes in the chemical composition of a molecule that are irreversible, giving rise to stable products. Reactions based-on elimination mechanisms have been proposed as the main pathways during pyrolysis ¹. Therefore, this particular idea has been extensively explored, by theoretical and experimental means, for simple organic compounds such as: carboxylic acid derivatives ^{2,3}, alkyl halides ⁴, ketals ⁵, and amino acids ^{6–8}. In the particular case of the latter, their pyrolysis has been subject of intensive study due to the increasing interest in the thermal decomposition of biomass at high temperature ⁶. Furthermore, it is important to point out that the biomass combustion leads to the production of environmentally harmful nitrogen containing polycyclic compounds ^{9,10} which differ in their identity and yield, depending on the temperature of the process, the residence time, and the chemical structure of the specific amino acids that are present in the protein composition of the biomass sample ¹¹.

The pyrolysis of amino acids form products based on reactions of dehydration, decarboxylation, or deamination, leading to common volatiles such as H₂O, NH₃, CO₂, CO, HNCO, y HCN ^{7,12}. However, formation of higher molecular weight products like 2,5-diketopiperazine (DKPs) compounds ^{7,11}, maleimide. succinimide, glutaramide, pirrolidone, and others ^{7,10} have been also observed as products during pyrolysis of these substrates. It has to be indicated that the formation of high molecular weight products from the pyrolysis of small organic compounds is not common in literature due to the decomposition nature of pyrolysis, which commonly imply an elimination reaction as commented before. Thus, the pyrolysis of amino acids represents a special case on these regards. Among the amino acids for which the formation of DKPs has

been reported, proline shows the highest production after pyrolysis at 300°C, resulting in a yield ca. 80% of the corresponding DKP^{8,13}. It is important to remark that, when pyrolysis is carried out for extended times, even the DKP is decomposed to form the aforementioned common volatile products¹⁴. In this sense, during the pyrolysis of proline, the final possible formation of ammonia and hydrogen cyanide, which are potentially toxic for human beings, has attracted the interest of the scientific community considering that this amino acid is commonly found in cigarettes¹⁵.

Previous theoretical studies of the proline pyrolysis mechanism have been centered on its unimolecular decomposition ¹⁶. Results obtained at the B3LYP/6-311g(2d,p) level of theory suggested that dehydration and decarboxylation reactions are the dominant unimolecular processes at a wide range of temperatures and pressures ¹⁶. However, the formation of DKP during the pyrolysis of proline at 300°C, has not been explored although the experimental results obtained from gas chromatography/mass spectrometry suggests its formation through a dimerization of proline ⁸. The objective of this work is to theoretically study the reaction mechanism for 2,5-diketopiperazine formation during the pyrolysis of proline at 300°C ¹⁷ and determine whether the formation of DKP is more favorable or not over the unimolecular decomposition.

2. COMPUTATIONAL METHODOLOGY

All the calculations were performed using the Gaussian 16 suit of programs ¹⁸. Geometry optimizations for all stationary points along the proposed mechanism (reactive, product, intermediates, and transition states) were calculated at DFT level of theory, using the wB97XD functional ¹⁹, and the 6-311g(d,p) basis set ^{20,21}. For the appropriate description of the transition state geometries, where differences of electronegativity and charge transfer could be important, a long-range dispersion-corrected functional was employed which has satisfactory accuracy for non-covalent

and non-bonded interactions¹⁹, while the selected basis set with polarization functions ensures to accurately describe the electronic configuration ²¹. Frequency calculations at 300°C were performed on the optimized molecules at the same level of theory, ensuring the existence of a unique imaginary eigenvalue in the Hessian matrix for transition states, and no imaginary eigenvalues for minimum energy configurations. The correlation of the corresponding transition vectors to the reaction pathway were also verified.

In order to analyze the thermodynamic properties of the mechanism, values of absolute enthalpies (H) were collected from the frequency output files from DFT calculations, while absolute Gibbs free energies were obtained using the Goodvibes v 2.0.3 program ²² which applies the quasi-harmonic approximation to the vibrational entropy and leads to quasi-harmonic corrected Gibbs free energies. The program was used by setting the temperature at 573.15 K, the approach proposed by Grimme in Ref. ²³, and the rest of parameters as default.

Degrees of rate control (X_{RC}) for all involved transition states were calculated according to the procedure described by Motagamwala ²⁴ (See Supplementary Information for details). Equation (1) is used to calculate the degree of rate control of the *i-th* transition state on a generalized sequence of n steps:

$$X_{RC,i} = \frac{\prod_{j=1, j \neq i}^{n} r_{max,j}}{\sum_{j=k}^{n} (\prod_{j=1, j \neq k}^{n} r_{max,j})}$$
(1)

Where $r_{max,i}$ is called the maximum rate of the *i-th* step, and is obtained according to equation (2):

$$r_{max,i} = \frac{k_B T}{h} K_{eq,A \to TS_i}^{\dagger} [CF]$$
(2)

Here, $K_{eq,A \to TS_i}^{\dagger}$ is a condensed constant which contains a combination of rate constants (k_j) and equilibrium constants (K_{eq,j}) of any elemental step involved in the

reaction pathway from the reactive to a *i-th* transition state. [CF] is a "concentration factor" which contains a combination of molar concentrations (or partial pressures in gas-phase reactions) of any reactive, product or by-product involved in the process. Neither $K_{eq,A\to TS_i}^{\dagger}$ nor [CF] have a general expression, and they have to be obtained for each particular case (check the Supplementary Information). k_B and h are the Boltzman's and Plank's constants, respectively, and T is the temperature of the process.

Additionally, the evolution of the DFT energy along the normalized reaction coordinate (ξ) between each stationary point was determined by Intrinsic Reaction Coordinate (IRC) calculations, and the profiles resulting for the rate controlling step were selected to a further detailed analysis by means of the reaction force formalism.

Reaction force (F(ξ)) profiles ^{25,26} were obtained numerically, according to equation (3):

$$F(\xi) = -\frac{dE}{d\xi}$$
(3)

By identifying the points on the reaction coordinates where critical points exist $(F(\xi) = 0)$, and the maximum and minimum of the reaction force, the reaction path can be divided in regions (j) in which geometrical and electronic rearrangements are dominant on each step (i) of interest. Upon region determination, values for works $(w_j^{(i)})$ are numerically calculated, from critical point *a* to critical point *b*, according to equation (4).

$$w_j^{(i)} = -\int_a^b F(\xi)d\xi \tag{4}$$

In order to obtain more detailed information about the mechanism, data of some selected geometrical parameters over the reaction coordinate were extracted from the IRC calculation outputs, which contain all the geometrical coordinates of atoms in each of the points plotting the IRC profile. A Natural Bond Orbital (NBO) calculation ²⁷ was also performed to gain additional insights on the process. Data associated to the charge on some selected atoms were extracted from NBO outputs of each of the corresponding stationary points involved in the determining reaction step. Subsequently, changes in the electronic distribution of each atom were quantified as a difference of charge, calculated for each of the atoms involved in the process, with equation (5).

$$\delta Q_{X \to Y}^{atom} = Q_Y^{atom} - Q_X^{atom} \tag{5}$$

Where $\delta Q_{X \to Y}^{atom}$ (or δQ for simplicity) is the difference of charge between stationary point X to stationary point Y, while Q_X^{atom} and Q_Y^{atom} are the NBO charge in each corresponding stationary point.

Similarly, from the corresponding NBO outputs, changes in Wiberg bond indexes ²⁸ were also analyzed to get more information. These changes were calculated as a fractional difference of bond order, using equation (6).

$$\delta B_{X \to Y}^{bond} = \frac{B_Y^{bond} - B_X^{bond}}{B_Z^{bond} - B_X^{bond}} \tag{6}$$

Where $\delta B_{X \to Y}^{bond}$ (or δB for simplicity) is the fractional difference of bond order between minimum X to the transition state Y, while B_X^{bond} , B_Y^{bond} and B_Z^{bond} are the Wiberg bond indexes in the corresponding stationary point: the minimum X, the transition state Y, and the following minimum Z.

Finally, the synchronicity ²⁹ of the step of interest was computed by using equation (7).

$$Sy = 1 - \frac{\sum_{i=1}^{n} |\delta B_i - \delta B_{average}|}{\delta B_{average} (2n-2)}$$
(7)

Where *Sy* is the synchronicity of a specific step, n is the number of bonds (only those bonds that change significantly are taken into account), δB_i is the fractional difference

of bond order for the i-esime bond, and $\delta B_{average}$ is the average of all δB_i taken into account.

3. RESULTS AND DISCUSSION

3.1. Mechanism of reaction and thermochemistry properties

Scheme 1 shows the mechanism for pyrolysis of proline studied in this work. This mechanism is based on the suggestion of Chiavari et al ⁸, who mentioned that after the proline dimerization (step 1), a double dehydration process (steps 2 and 4) and cyclization (step 3) lead to the DKP product (P).



Scheme 1. Reaction mechanism proposed for proline pyrolysis

Each stationary point (reactant, transition states, intermediates and product) was separately optimized, and the differences of enthalpy between each pair of points were calculated using the absolute thermochemical values obtained from DFT frequency calculations (see Table 1). With these data, a reaction profile based on normalized enthalpies is shown in Figure 1.

 Table 1. Thermodynamic parameters calculated from absolute enthalpies and entropies

 obtained through the DFT calculation: wb97xd/6-311g(d,p)

i	X	Y	$\begin{array}{c} \Delta H_i \\ H_Y^{DFT} - H_X^{DFT} \\ (\text{kJ mol}^{-1}) \end{array}$	Normalized Enthalpy H_Y (kJ mol ⁻¹)
		2 R		0.0
1	2 R	TS1	129.2	129.2
-1	TS1	INT1	-145.2	-16.0
2	INT1	TS2	174.2	158.2
-2	TS2	INT2+H ₂ O	-153.8	4.4
3	INT2+H ₂ O	TS3	113.8	118.1
-3	TS3	INT3	-133.7	-15.6
4	INT3	TS4	108.2	92.7
-4	TS4	P+H ₂ O	-142.5	-49.9
N	Inter Tan	anaratura	used for	the DET

Note: Temperature used for the DFT calculations was 573.15 K



Figure 1. Enthalpy profile for the formation of 2,5-diketopiperazine product through a dimerization process. Structures of TS in the top of the figure are the optimized geometries.

Although INT1 and INT3 are more stable than the reactive (2R), all intermediates are unstable when compared with the product (P); therefore, the global reaction is exothermic ($\Delta H_{reaction} = -49.9$ kJ/mol). Additionally, since the change in the Gibbs free energy for the global reaction is negative ($\Delta G_{reaction} = -110.9$ kJ/mol), it can be stablished that the process is spontaneous.

From the differences of barriers of Figure 1, it can be assumed that the main processes of the reaction depends on the first two steps: the dimerization of proline, and the subsequent elimination of a molecule of water. After that, it appears that faster steps consisting in a less energy-demanding cyclization and a second elimination of water will finally form the 2,5-diketopiperazine product. In these regards, the details about the determination of the degree of rate control for this particular reaction mechanism are presented in the next section.

3.2.Determination of the degrees of rate control

In order to describe the kinetic properties of the proposed mechanism, the following reaction steps and rate constants are considered:

$$2R \xrightarrow[k_{-1}]{k_{-1}} INT1 \qquad (8)$$

$$INT1 \xrightarrow[k_{-2}]{k_{-2}} INT2 + H_2O \qquad (9)$$

$$INT2 \xrightarrow[k_{-3}]{k_{-3}} INT3 \qquad (10)$$

$$INT3 \xleftarrow[k_{-4}]{k_{-4}} P + H_2O \qquad (11)$$

Now, according to Motagamwala ²⁴, the degrees of rate control (X_{RC}) for transition states can be calculated using equations (1) and (2) (See details in Supporting Information). Results are summarized in Table 2:

Table 2. Rate constants, equilibrium constants, maximum rates, and degrees of ratecontrol for elementary steps on the mechanism of formation of 2,5-diketopiperazine from pyrolysis of proline

i	$\frac{k_i}{\frac{k_B T}{h}} e^{-\frac{\Delta G_i^{qh}}{RT}}$ (s ⁻¹)	$K_{eq,i} \ k_i/k_{-1}$ (dimensionless)	Expression for $r_{max,i}$	$r_{max,i}$ eq.(2) (s ⁻¹)	X _{RC,i} eq.(1) (dimensionless)
1	1.10×10^{-10}	4.59×10^{-10}	$k_1[R]^2$	1.10×10^{-10}	4.14×10^{-3}
-1	2.39×10^{-1}				
2	9.94×10^{-4}	9.81×10 ⁶	$k_{eq,1}k_2[R]^2$	4.56×10^{-13}	9.96×10^{-1}
-2	1.01×10^{-10}				
3	1.82×10^{-1}	5.03×10 ⁰	$k_{eq,1}k_{eq,2}k_3 [R]^2 [H_2 O]^{-1}$	8.22×10^{-2}	5.53×10 ⁻¹²
-3	3.63×10^{-0}				
4	1.83×10^{-3}	5.19×10 ¹¹	$k_{eq,1}k_{eq,2}k_{eq,3}k_4[R]^2[H_2O]^{-1}$	4.14×10^{-1}	1.10×10^{-14}
-4	3.53×10^{-9}				

Note: For the determination of rate constants (k_i), quasi-harmonic corrected Gibbs free energies (ΔG_i^{qh}) were obtained by using the Goodvibes v 2.0.3 program. The temperature (T) used in calculations was 573.15 K. k_B and h are the Boltzman's and Plank's constants, respectively.

These degrees of rate control represent an indicator of how much influence has a transition state on the total reaction rate. The farther the $X_{RC,i}$ from zero the more significant the influence in the rate of the reaction is higher. The sum of all X_{RC} must be the unity.

From the calculated values, TS2 corresponds to the most influent transition state on the reaction rate with a $X_{RC,TS2} = 0.996$, while the rest of $X_{RC,i}$ are almost zero. Looking at the minimum configurations, INT1, which precedes TS2, represents the most stable intermediate in the profile. The energy barrier formed from INT1 to TS2 is the highest one. Therefore, the second elemental step of the mechanism, the dehydration process, can be suggested as the most important step on the rate of the process.

It is interesting to notice that the second dehydration (the fourth step), is not as important to the reaction rate as the first one. Considering that the molecule has lost a rotational degree of freedom when it becomes a cycle, the second dehydration should be less geometrically demanding, and therefore, more favored than the first dehydration.

3.3.Determination of the overall activation energy

Although the first dehydration process (from INT1 to TS2) contains the rate determinant states of the mechanism as indicated in the last section, due to the fact that formation of INT1 is exothermic and contributes with approximately 16 kJ/mol to the reaction energy, the net energetic barrier should be corrected by subtracting this value to the activation energy of the dehydration; in other words, the net energy of the reaction should be considered as the difference of enthalpy from 2R to INT2. Whit the last consideration, it can be stablished that the global reaction needs to overcome an activation enthalpy (ΔH^{\ddagger}) of 158.2 kJ/mol.

The dimerization mechanism presented in this work is compared with the unimolecular decomposition of this substrate, which was previously theoretically studied by Rawadieh et al ¹⁶. According to Rawadieh, the unimolecular process during pyrolysis of proline involve a direct dehydration of this amino acid ¹⁶, as depicted in Scheme 2.



Scheme 2. Reaction for the most favored unimolecular process during proline pyrolysis, according to Rawadieh et al.

An activation enthalpy of 315.7 kJ/mol was calculated by us for this reaction at the wB97XD/6-311G(d,p) level, which is in agreement with the reported value of 297.1 kJ/mol (71.0 kcal/mol) obtained by Rawadieh at the B3LYP/6-311G(2d,p) level ¹⁶. By comparing this barrier against the DKP formation (158.2 kJ/mol), it is possible to conclude that the dimerization is favored, with a requirement of approximately half of

the energy needed for the mentioned unimolecular reaction. This difference in activation barrier allows us to explain why the DKP product is the main compound in low temperature pyrolysis 8 .

3.4.Electronic energy through the intrinsic reaction coordinate (IRC), reaction forces (RF), and works (w)

The electronic energy over the reaction coordinate from 2R to INT2 is studied. Specifically, the barriers governed by k_2 (INT1 \rightarrow TS2) and k_{-1} (INT1 \rightarrow TS1) are analyzed using the reaction force approach (see Figure 2). The involved works $(w_j^{(i)})$ were calculated by numerical integration of the area under the curve for each region (j) of each reaction step (i) in the reaction force plot.



Figure 2. Total electronic energy through the reaction coordinate of the two elemental steps involved in the formation of the dipeptide of Proline: dimerization step (left) and dehydration step (right); and their corresponding Reaction Force plots (first derivative of the energy) and works (area under the curve). Work's values are in kJ/mol.

Due to the fact that absolute values of works corresponding to so-called geometrical interactions $(w_{IV}^{(1)} \text{ and } w_{I}^{(2)})$ are higher than those corresponding to electronic ones $(w_{III}^{(1)} \text{ and } w_{II}^{(2)})$, the conversion of INT1 to whether INT2 or 2R, is predominantly dominated by the geometry rearrangement of the molecule, which in both cases represent approximately 75% of the energy needed to overcome the barrier. It could be related to the fact that INT1 is the most influent intermediate to the rate of the reaction as mentioned earlier.

3.5.Geometrical parameters of INT1 through the reaction coordinate

For both, forward and reverse directions from INT1, the geometrical changes of the molecule are analyzed (see Figure 3).



Figure 3. Change in the bond angle between atoms N–C–O from TS1 to INT1 (left), and between atoms O–C–O from INT1 to TS2 (right).

In order to achieve TS2 to dehydrate the dimer, INT1 requires the approximation of the alcohol groups in order to obtain an oxygen-to-oxygen proton transfer. This is achieved by decreasing the O–C–O angle from 107° to 93°, and keeping this latter value during the proton transfer. C-O and O-H distances are practically kept constant upon completion of the proton transfer, then these bonds rapidly change from 1.40 to 1.62 Å, and from 0.96 to 1.34 Å, respectively. Notice that the C-O bond starts to break a few earlier than the O-H bond.

In the reverse path, the angle between the N–C–O in INT1 decreases from 109° to 93° in order to form the initial proline molecules; thus, the proton transfer (from oxygen to nitrogen), and the rupture of the dimer, can be achieved. Looking at the N-C and O-H distances, a similar behavior than in forward direction can be seen: the proton transfer occurs at the end changing O-H distance from 0.96 to 1.32 Å, while the N-O bond rupture starts a few earlier with a change from 1.47 to 1.66 Å.

3.6. Charge distribution and bond order changes from INT1 to TS2

TS2 is a transition state of four members (see Figure 4) where the oxygen atoms are rich in electronic density while the carbon and hydrogen atoms are deficient.



Figure 4. Optimized structure of TS2, showing the four atoms involved in the process of dehydration. Oxygen atoms have been labelled as O(1) and O(2) to differentiate them.

Focusing on the differences between TS2 and INT1, the changes in electronic distribution were quantified as a difference of charge ($\delta Q_{INT1 \rightarrow TS2}^{atom}$, or δQ for simplicity), calculated for each of the four atoms involved in the process, with the

equation (5). All values obtained for δQ (see Table 3) belongs on the range between - 0.09 to 0.06; those relatively small values suggest that charge transfer is not an important parameter to achieve TS2, which is coherent with the reaction force analysis where geometric rearrangement is the most important factor.

Table 3. Electronic density for selected atoms and change in the charge

	O (1)	Η	O(2)	С
INT1	-0.78	0.48	-0.78	0.77
TS2	-0.87	0.54	-0.80	0.80
$\partial Q_{INT1 \rightarrow T}^{atom}$	-0.09	0.06	-0.03	0.02

By analyzing the changes in Wiberg bond indexes of TS2 respect to INT1 (see Table 4), the fractional difference of bond order ($\delta B_{INT1\to TS2}^{bond}$, or δB for simplicity) was calculated using the equation (6). When a bond is broken or formed between two intermediates, δB represents a measure of how much that bond have been transformed when the reaction reached the corresponding transition state; a $\delta B = 0$ means that the bond has not changed during the process, while a $\delta B = 1$ means a complete bond conversion. Additionally, Table 4 shows: the average of all δB , which lets estimate if the transition state is an early TS ($\delta B_{average} < 0.5$), or a late TS ($\delta B_{average} > 0.5$); and the synchronicity of the step, as defined by equation (7), which represents how synchronous is the process.

Table 4. Wiberg bond indexes for selected bonds and change in the charge distribution

	O(1) H	O (2) – – C	O(2) H	O(1) =-= C	$\delta B_{average}$	Sy
INT1	0.752	0.943	0.003	0.897	-	-
TS2	0.262	0.626	0.422	1.160	-	-
INT2	0.005	0.006	0.778	1.646	-	-
$\partial B^{bond}_{INT1 o TS2}$	0.656	0.339	0.541	0.352	0.472	0.821
	single- bond	single-bond	single-bond	double-bond		
	rupture	rupture	formation	formation		

Values of δB in Table 4 show that the O(1)–H rupture and the O(2)–H formation are the principal electronic rearrangements that occur to achieve TS2, while C–O(2) rupture and C=O(1) formation are mainly completed after the TS. This observation proves that, due to the known instability of hydroxyl anions, water molecule is mostly formed first, and then it is separated from the molecule matrix. Additionally, the $\delta B_{average} = 0.472$ means that TS2 is an early transition state, which corresponds well with the intrinsic coordinate (< 0.5) where TS2 is located (see Figure 2). Finally, the value for synchronicity (Sy = 0.821) express that the process is non synchronous, which represents a TS in a concerted slightly polar process.

4. CONCLUSIONS

The dominancy of the geometrical type rearrangements needed to achieve weather TS2 or TS1, along with the high activation energies in both ways, makes INT1 a very stable intermediate. However, since INT1 is more energetic than P, it keeps as an intermediate in the process. With these information, it can be understood the fact that the dehydration step, which contains both rate controlling states (INT1 and TS2), is the most influent step on the rate of the mechanism. Here, the geometrical rearrangements needed to achieve TS2 are dominated by the approximation of the oxygen atoms involved in the proton transfer, while electronic rearrangements depend on the almost formation of the molecule of water just before its separation from the molecular matrix. Electronic rearrangements do not need a significant charge transfer, possibly because the process is slightly asynchronous because rupture and formation of bonds occur almost at the same time.

ASSOCIATED CONTENT

Supporting Information

Additional information is available free of charge. This material contains: A) A detailed development for the determination of degrees of rate control; B) The optimized geometries of each transition state of the profile; C) DFT energy through the intrinsic reaction coordinate (IRC) for each step of the mechanism.

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SUPPORTING INFORMATION

A. Development of the determination of degrees of rate control

According to Motagamwala¹, degrees of rate control (X_{RC}) for transition states can be calculated by the following procedure:

Considering the following four-step reaction scheme:

(1)
$$2R \xrightarrow[k_{-1}]{k_{-1}} INT1$$

(2) $INT1 \xrightarrow[k_{-2}]{k_{-2}} INT2 + H_2O$
(3) $INT2 \xrightarrow[k_{-3}]{k_{-3}} INT3$
(4) $INT3 \xrightarrow[k_{-4}]{k_{-4}} P + H_2O$

The reversibility of step i (Zi) is defined as the rate of the reverse reaction divided by the rate of the forward reaction:

$$Z_{1} = \frac{r_{-1}}{r_{1}} = \frac{k_{-1}[INT1]}{k_{1}[R]^{2}} = \frac{[INT1]}{K_{eq,1}[R]^{2}}$$

$$Z_{2} = \frac{r_{-2}}{r_{2}} = \frac{k_{-2}[INT2][H_{2}O]}{k_{2}[INT1]} = \frac{[INT2][H_{2}O]}{K_{eq,2}[INT1]}$$

$$Z_{3} = \frac{r_{-3}}{r_{3}} = \frac{k_{-3}[INT3]}{k_{3}[INT2]} = \frac{[INT3]}{K_{eq,3}[INT2]}$$

$$Z_{4} = \frac{r_{-4}}{r_{4}} = \frac{k_{-4}[P][H_{2}O]'}{k_{4}[INT3]} = \frac{[P][H_{2}O]'}{K_{eq,4}[INT3]}$$

From these equations, concentrations of the intermediates can be obtained:

$$[INT1] = Z_1 K_{eq,1} [R]^2$$
$$[INT2] = Z_2 K_{eq,2} \frac{[INT1]}{[H_2 O]} = Z_1 Z_2 K_{eq,1} K_{eq,2} \frac{[R]^2}{[H_2 O]}$$
$$[INT3] = Z_3 K_{eq,3} [INT2] = Z_1 Z_2 Z_3 K_{eq,1} K_{eq,2} K_{eq,3} \frac{[R]^2}{[H_2 O]}$$

The reversibility of the overall reaction (β) is also obtained:

$$\begin{split} \beta &= Z_1 Z_2 Z_3 Z_4 = \frac{[INT1]}{K_{eq,1} [R]^2} \frac{[INT2] [H_2 O]}{K_{eq,2} [INT1]} \frac{[INT3]}{K_{eq,3} [INT2]} \frac{[P] [H_2 O]'}{K_{eq,4} [INT3]} \\ \beta &= \frac{[P] [H_2 O] [H_2 O]'}{K_{eq,1} K_{eq,2} K_{eq,3} K_{eq,4} [R]^2} \end{split}$$

After that, it is possible to write expressions for the net rate of each step, considering that the net rates of all elementary steps are equal to the net rate of the overall reaction:

$$r = r_{1} - r_{-1} = r_{1}(1 - Z_{1}) = k_{1}[R]^{2}(1 - Z_{1})$$

$$r = r_{2} - r_{-2} = r_{2}(1 - Z_{2}) = k_{2}[INT1](1 - Z_{2}) = K_{eq,1}k_{2}[R]^{2}Z_{1}(1 - Z_{2})$$

$$r = r_{3} - r_{-3} = r_{3}(1 - Z_{3}) = k_{3}[INT2](1 - Z_{3}) = K_{eq,1}K_{eq,2}k_{3}\frac{[R]^{2}}{[H_{2}O]}Z_{1}Z_{2}(1 - Z_{3})$$

$$r = r_{4} - r_{-4} = r_{4}(1 - Z_{4}) = k_{4}[INT3](1 - Z_{4}) = K_{eq,1}K_{eq,2}K_{eq,3}k_{4}\frac{[R]^{2}}{[H_{2}O]}Z_{1}Z_{2}Z_{3}\left(1 - \frac{\beta}{Z_{1}Z_{2}Z_{3}}\right)$$

Where the concentrations of the intermediates have been replaced by their corresponding expressions in terms of concentrations of reactive, product, and byproducts. Z_4 was also replaced by the reversibility of the overall reaction (β) and the reversibilities of steps 1, 2, and 3.

It can be noticed that the net rates are controlled by the four following lumped parameters, Ci:

$$C_{1} = k_{1} = \nu^{\dagger} k_{TS_{1}}^{\dagger} = \frac{k_{B}T}{h} K_{eqR \to TS_{1}}^{\dagger}$$

$$C_{2} = K_{eq,1} k_{2} = \nu^{\dagger} K_{eq,1} k_{TS_{2}}^{\dagger} = \frac{k_{B}T}{h} K_{eqR \to TS_{2}}^{\dagger}$$

$$C_{3} = K_{eq,1} K_{eq,2} k_{3} = \nu^{\dagger} K_{eq,1} K_{eq,2} k_{TS_{3}}^{\dagger} = \frac{k_{B}T}{h} K_{eqR \to TS_{3}}^{\dagger}$$

$$C_{4} = K_{eq,1} K_{eq,2} K_{eq,3} k_{4} = \nu^{\dagger} K_{eq,1} K_{eq,2} K_{eq,3} k_{TS_{4}}^{\dagger} = \frac{k_{B}T}{h} K_{eqR \to TS_{4}}^{\dagger}$$

Where the expression $k_i = v^{\dagger} k_{TS_i}^{\dagger}$ has been used according to transition state theory: the rate constant of step i is expressed in terms of a frequency factor ($v^{\dagger} = k_B T/h$) times the equilibrium constant for the formation of the transition state.

The condensation of all constants into $K_{eqR \to TS_i}^{\dagger}$ represents the equilibrium constant for the formation of the transition state for step i from the reactant R.

To assess if an elementary step may contribute significantly to a reaction scheme, the maximum rate of this step can be estimated. This maximum rate corresponds to the case where the reversibility of step i is equal to the overall reversibility (β), while the rest of reversibilities of the other steps are equal to zero. Thus, if $Z_i = \beta$ and $Z_{j \neq i} = 1$:

$$r_{1} = \frac{k_{B}T}{h} K_{eqR \to TS_{1}}^{\dagger} [R]^{2} (1 - \beta) = r_{max,1} (1 - \beta)$$

$$r_{2} = \frac{k_{B}T}{h} K_{eqR \to TS_{2}}^{\dagger} [R]^{2} (1 - \beta) = r_{max,2} (1 - \beta)$$

$$r_{3} = \frac{k_{B}T}{h} K_{eqR \to TS_{3}}^{\dagger} \frac{[R]^{2}}{[H_{2}O]} (1 - \beta) = r_{max,3} (1 - \beta)$$

$$r_{4} = \frac{k_{B}T}{h} K_{eqR \to TS_{4}}^{\dagger} \frac{[R]^{2}}{[H_{2}O]} (1 - \beta) = r_{max,4} (1 - \beta)$$

Here, it can be generalized an expression for $r_{max,i}$, as follows:

$$r_{max,i} = \frac{k_B T}{h} K_{eq,A \to TS_i}^{\dagger} [CF] \tag{1}$$

Where [CF] represents the concentration factor which is different for each step, as can be seen above in each specific expression of $r_{max,i}$.

Now, in order to estimate the degrees of rate control for each step, it is necessary to solve the expressions of reversibilities (Z_i) in terms of the maximum rates ($r_{max,i}$).

Noticing that the net rates of all steps are equal to the net rate of the overall reaction, we have:

$$r = r_{max,1}(1 - Z_1)$$

$$r = r_{max,2}Z_1(1 - Z_2)$$

$$r = r_{max,3}Z_1Z_2(1 - Z_3)$$

$$r = r_{max,4}Z_1Z_2Z_3\left(1 - \frac{\beta}{Z_1Z_2Z_3}\right)$$

The following expressions for reversibilities can be obtained:

$$Z_{1} = \frac{r_{max,1}r_{max,2}r_{max,3} + \beta r_{max,2}r_{max,3}r_{max,4} + r_{max,3}r_{max,4}r_{max,1} + r_{max,4}r_{max,1}r_{max,2}}{r_{max,1}r_{max,2}r_{max,3} + r_{max,2}r_{max,3}r_{max,4} + r_{max,3}r_{max,4}r_{max,1} + r_{max,4}r_{max,1}r_{max,2}}$$

$$Z_{2} = \frac{r_{max,1}r_{max,2}r_{max,3} + \beta r_{max,2}r_{max,3}r_{max,4} + \beta r_{max,3}r_{max,4}r_{max,1} + r_{max,4}r_{max,1}r_{max,2}}{r_{max,1}r_{max,2}r_{max,3} + \beta r_{max,2}r_{max,3}r_{max,4} + r_{max,3}r_{max,4}r_{max,1} + r_{max,4}r_{max,1}r_{max,2}}$$

$$Z_{3} = \frac{r_{max,1}r_{max,2}r_{max,3} + \beta r_{max,2}r_{max,3}r_{max,4} + \beta r_{max,3}r_{max,4}r_{max,1} + \beta r_{max,4}r_{max,1}r_{max,2}}{r_{max,1}r_{max,2}r_{max,3} + \beta r_{max,2}r_{max,3}r_{max,4} + \beta r_{max,3}r_{max,4}r_{max,1} + r_{max,4}r_{max,1}r_{max,2}}$$

The next phase is to express the degree of rate control in terms of $r_{max,i}$. Considering the definition of the degree of rate control for step i ($X_{RC,i}$):

$$X_{RC,i} = \left(\frac{\partial r}{\partial k_i}\right) \frac{k_i}{r} \Big|_{K_{eq,i}k_{j\neq i}}$$
(2)

While the sensitivity, s_i , for each step is defined as:

$$s_i = \left(\frac{\partial r}{\partial k_i}\right) \frac{k_i}{r} \Big|_{k_{j \neq i}} \tag{3}$$

Thus, the degree of rate control can be expressed as follows:

$$X_{RC,i} = s_i (1 - Z_i) \tag{4}$$

And, for each step of the reaction scheme, degrees of rate control in terms of the sensitivity can be written as:

$$\begin{aligned} X_{RC,1} &= s_1(1 - Z_1) \\ X_{RC,2} &= s_1 Z_1 (1 - Z_2) \\ X_{RC,3} &= s_1 Z_1 Z_2 (1 - Z_3) \\ X_{RC,4} &= s_1 Z_1 Z_2 Z_3 \left(1 - \frac{\beta}{Z_1 Z_2 Z_3} \right) \end{aligned}$$

Finally, the values of Z_i can then be expressed in terms of $r_{max,i}$, and the value of s_1 is obtained by requiring that the sum of $X_{RC,i}$ be equal to unity, leading to the following result:

$$X_{RC,1} = \frac{r_{max,2}r_{max,3}r_{max,4}}{r_{max,2}r_{max,3}r_{max,4} + r_{max,1}r_{max,3}r_{max,4} + r_{max,1}r_{max,2}r_{max,4} + r_{max,1}r_{max,2}r_{max,3}r_{max,3}}$$
$$X_{RC,2} = \frac{r_{max,1}r_{max,3}r_{max,4}}{r_{max,2}r_{max,3}r_{max,4} + r_{max,1}r_{max,2}r_{max,4} + r_{max,1}r_{max,2}r_{max,3}r_{max,4}}$$

Which can be generalized as follows:

$$X_{RC,i} = \frac{\prod_{j=1,j\neq i}^{n} r_{max,j}}{\sum_{j=k}^{n} (\prod_{j=1,j\neq k}^{n} r_{max,j})}$$
(5)

Therefore, by determining the rate constants from values of enthalpy and entropy from DFT calculations, and using the presented equations, results for degrees of rate control for the present reaction scheme are shown in Table 1. Due to the fact that the process is carried oud in gas-phase, concentrations [R] and [H₂O] are replaced by the partial pressures P_R and P_{H2O} , and both are considered as 1 atm.

 Table 1. Rate constants, equilibrium constants, maximum rates, and degrees of rate-control for elementary steps on the mechanism of formation of 2,5-diketopiperazine from pyrolysis of proline

i	$\frac{k_i}{\frac{k_B T}{h}} e^{-\frac{\Delta G_i^{qh}}{RT}}$ (s ⁻¹)	$K_{eq,i}$ k_i/k_{-1} (dimensionless)	Expression for $r_{max,i}$	$r_{max,i}$ eq.(2) (s ⁻¹)	X _{RC,i} eq.(1) (dimensionless)
1	1.10×10^{-10}	4.59×10^{-10}	$k_1[R]^2$	1.10×10^{-10}	4.14×10^{-3}
-1	2.39×10^{-1}				
2	9.94×10^{-4}	9.81×10 ⁶	$k_{eq,1}k_2[R]^2$	4.56×10 ⁻¹³	9.96×10 ⁻¹
-2	1.01×10^{-10}				
3	1.82×10^{-1}	5.03×10^{0}	$k_{eq,1}k_{eq,2}k_3 [R]^2 [H_2 O]^{-1}$	8.22×10^{-2}	5.53×10 ⁻¹²
-3	3.63×10^{0}				
4	1.83×10 ³	5.19×10 ¹¹	$k_{eq,1}k_{eq,2}k_{eq,3}k_4[R]^2[H_2O]^{-1}$	4.14×10 ¹	1.10×10^{-14}
-4	3.53×10 ⁻⁹				

Note: For the determination of rate constants (k_i) , quasi-harmonic corrected Gibbs free energies (ΔG_i^{qh}) were obtained by using the Goodvibes v 2.0.3 program. The temperature (T) used in calculations was 573.15 K. k_B and h are the Boltzman's and Plank's constants, respectively.

B. Cartesian coordinates for each of the optimized transition states

Geometry of transition states were optimized by Gaussian calculations² at DFT wb97xd/6-311g(d,p) level of theory. The corresponding Cartesian coordinates of each structure, denoted as TS_i (see Scheme 1 in the main document), are presented as follows:

TS1 TS2 Coordinates (Angstroms) Coordinates (Angstroms) Atom Atom symbol symbol Х Y Ζ Х Y Ζ Ν 1.758733 0.386769 1.036967 Ν -1.889674 0.483554 -0.897440

C	3.153479	0.865096	1.091220
С	1.425397	-0.015268	-0.330899
Η	3.739095	0.221833	1.756431
Η	3.210116	1.883068	1.486321
С	3.671015	0.769676	-0.350511
С	2.787437	-0.318044	-0.959824
Η	0.945063	0.787049	-0.908766
С	0.529263	-1.261359	-0.334767
Η	4.736461	0.538731	-0.400850
Η	3.507498	1.717449	-0.873715
Η	3.115960	-1.311942	-0.643905
Η	2.742700	-0.310009	-2.047456
0	0.834429	-2.058828	0.738900
0	0.367439	-1.877355	-1.492152
Ν	-1.092977	-0.922774	-0.181628
С	-1.850407	-1.273930	1.034510
С	-1.682102	0.275007	-0.766830
Η	-1.313809	-0.910370	1.911128
Η	-1.920455	-2.358422	1.100443
С	-3.219383	-0.580028	0.870998
С	-3.187276	0.032684	-0.540340
Η	-1.410222	0.315185	-1.826335
С	-1.280979	1.574111	-0.074236
Η	-3.332443	0.204462	1.620685
Η	-4.051327	-1.275058	0.986994
Η	-3.789474	0.939309	-0.630061
Η	-3.535395	-0.683769	-1.287527
0	-0.919819	1.655936	1.065342
0	-1.427054	2.684871	-0.818521
Η	1.091682	1.051422	1.405095
Η	-0.872333	-1.715263	-1.081538
Η	-1.690469	2.458567	-1.714334
Η	1.248446	-1.444869	1.375540

TS3

Atom	Coordi	nates (Angs	troms)
symbo	I X	Y	Z
N	-1.211564	-0.482878	0.214628
С	-2.524416	-1.065533	-0.073965
С	-1.188364	0.804343	-0.496583
Η	-2.753191	-1.840610	0.655608
Н	-2.500658	-1.528764	-1.066354
С	-3.469411	0.153957	-0.030178
С	-2.551712	1.397573	-0.175686
Н	-1.108748	0.592185	-1.574403
С	0.047490	1.587997	-0.072719
Н	-4.014147	0.186574	0.914039
Н	-4.208638	0.095967	-0.830170
Н	-2.484038	1.961348	0.755719
Н	-2.884524	2.086613	-0.951150
0	0.011998	2.739454	0.311583
Ν	1.169745	0.840337	-0.169955
С	2.471368	1.303258	0.300093
С	1.171469	-0.564396	-0.576190
Н	2.482243	1.322274	1.394790
Н	2.666411	2.312790	-0.063237
С	3.422128	0.244990	-0.255288

С	-3.083261	1.245428	-0.541401
С	-1.332926	0.022578	0.374498
Н	-3.712579	1.411415	-1.417799
Н	-2.824195	2.227179	-0.116499
С	-3.747109	0.359825	0.521058
С	-2.573550	-0.406790	1.175056
Н	-0.837959	0.839953	0.917158
С	-0.300442	-1.100586	0.132322
Н	-4.440102	-0.338504	0.046768
Н	-4.318041	0.948972	1.240189
Η	-2.710191	-1.486352	1.116959
Η	-2.449481	-0.169376	2.231552
0	-0.948983	-1.935691	-1.093834
0	-0.318532	-2.134760	0.951327
Ν	0.946163	-0.604386	-0.357622
С	1.922029	-1.637556	-0.736376
С	1.602140	0.440576	0.409350
Η	2.188151	-1.517139	-1.791510
Η	1.491030	-2.626435	-0.594070
С	3.123218	-1.393506	0.169918
С	3.113058	0.124744	0.306513
Н	1.312099	0.405054	1.471802
С	1.305366	1.851599	-0.098510
Н	4.059480	-1.776832	-0.238990
Η	2.945530	-1.860794	1.142619
Η	3.530464	0.590384	-0.591710
Η	3.675148	0.488605	1.169917
0	0.623311	2.132515	-1.039363
0	1.895227	2.830199	0.619769
Η	-1.200038	1.035043	-1.400844
Η	-0.983649	-2.561745	-0.134303
Η	2.416549	2.453435	1.333603
Η	-1.716966	-1.393023	-1.377162

TS4

Atom symbo	Coordi I X	nates (Angs Y	troms) Z
 N	-1 208425	-0 565393	-0 494953
C	-2.479649	-1.091495	0.023185
Č	-1.230228	0.903461	-0.615990
Н	-2.322166	-1.374415	1.067298
Н	-2.785650	-1.969429	-0.544503
С	-3.427096	0.098568	-0.109056
С	-2.511815	1.304257	0.111365
Н	-1.291093	1.169523	-1.679872
С	0.025725	1.569916	-0.052059
Н	-4.243184	0.050049	0.612054
Н	-3.863260	0.128389	-1.112295
Н	-2.288206	1.434928	1.172406
Η	-2.916559	2.242565	-0.264809
0	-0.014150	2.642371	0.515605
Ν	1.164789	0.881723	-0.284952
С	2.440090	1.262109	0.312435
С	1.164079	-0.491183	-0.778121
Н	2.356436	1.245608	1.405142
Н	2.715390	2.274162	0.013965
С	3.391485	0.183796	-0.205620

С	2.583120	-1.036351	-0.219878	С	2.503825	-1.061247	-0.314741
Н	0.987851	-0.633074	-1.661273	Н	1.111849	-0.500229	-1.877754
С	0.094447	-1.361528	0.202234	С	-0.072904	-1.217756	-0.301297
Η	4.338276	0.163319	0.330579	Н	4.246514	0.033846	0.454129
Η	3.698133	0.495298	-1.284235	Н	3.772393	0.466813	-1.191305
Н	2.544543	-1.442490	0.793805	Н	2.367402	-1.526292	0.661484
Η	2.944072	-1.811140	-0.896605	Н	2.888933	-1.811773	-1.003907
0	0.250854	-1.397798	1.513736	0	-0.084399	-2.526739	-0.178670
0	-0.131515	-2.606330	-0.383258	0	0.184555	-1.300202	1.693039
Η	-0.806811	-0.588836	1.353706	Н	0.165148	-2.448073	0.862448
Η	0.004550	-2.542138	-1.331044	Н	0.882370	-0.915975	2.224474

C. Electronic energy through the intrinsic reaction coordinate (IRC) for each step of the mechanism

Gaussian calculations² to determine the electronic energy from each transition state to both, forward and reverse directions over the corresponding reaction coordinate, were developed. The normalized data is presented, as follows:

		- 0.015117	2.186372	0.032934	5.018147
Intrinsic	Electronic	0.015657	2.268130	0.033473	5.108417
Coordinate	Energy	0.016197	2.350140	0.034013	5.198965
	(kJ/mol)	0.016737	2.432400	0.034553	5.289794
		- 0.017276	2.514909	0.035093	5.380902
0.000000	0.000000	0.017816	2.597667	0.035633	5.472290
0.000540	0.074619	0.018356	2.680675	0.036173	5.563965
0.001080	0.149499	0.018896	2.763935	0.036713	5.655923
0.001619	0.224635	0.019436	2.847441	0.037253	5.748170
0.002160	0.300032	0.019976	2.931200	0.037792	5.840703
0.002699	0.375688	0.020516	3.015211	0.038332	5.933528
0.003239	0.451602	0.021056	3.099471	0.038872	6.026644
0.003779	0.527773	0.021596	3.183981	0.039412	6.120048
0.004319	0.604201	0.022135	3.268745	0.039952	6.213750
0.004859	0.680889	0.022676	3.353759	0.040492	6.307745
0.005399	0.757832	0.023215	3.439027	0.041032	6.402038
0.005938	0.835032	0.023755	3.524547	0.041572	6.496626
0.006479	0.912490	0.024295	3.610322	0.042112	6.591512
0.007018	0.990202	0.024835	3.696352	0.042652	6.686697
0.007558	1.068172	0.025375	3.782637	0.043192	6.782184
0.008098	1.146396	0.025915	3.869181	0.043731	6.877970
0.008638	1.224877	0.026455	3.955980	0.044271	6.974055
0.009178	1.303611	0.026995	4.043039	0.044811	7.070445
0.009718	1.382599	0.027534	4.130358	0.045351	7.167135
0.010258	1.461839	0.028074	4.217939	0.045891	7.264128
0.010798	1.541334	0.028614	4.305783	0.046431	7.361424
0.011338	1.621083	0.029154	4.393890	0.046971	7.459024
0.011877	1.701085	0.029694	4.482261	0.047511	7.556924
0.012418	1.781336	0.030234	4.570901	0.048050	7.655131
0.012957	1.861842	0.030774	4.659808	0.048591	7.753640
0.013497	1.942597	0.031314	4.748983	0.049130	7.852450
0.014037	2.023604	0.031854	4.838432	0.049670	7.951563
0.014577	2.104863	0.032394	4.928153	0.050210	8.050980

Step 1: $2R \rightarrow TS1 \rightarrow INT1$

0.050750	8.150697	0.083144	14.665111	0.115538	22.294727
0.051290	8.250715	0.083684	14.782660	0.116077	22.431805
0.051830	8.351035	0.084223	14.900521	0.116617	22.569202
0.052369	8.451655	0.084764	15.018700	0.117157	22.706920
0.052910	8.552574	0.085303	15.137197	0.117697	22.844956
0.053450	8.653790	0.085843	15.256014	0.118237	22.983315
0.053989	8.755305	0.086383	15.375149	0.118777	23.121991
0.054530	8.857116	0.086923	15.494604	0.119317	23.260990
0.055069	8 959225	0.087463	15 614381	0 119857	23 400310
0.055609	9.061627	0.088003	15 734480	0 120397	23 539949
0.056149	9 164324	0.088543	15 854904	0.120936	23.679915
0.056689	0.267314	0.0800943	15.075653	0.120/30	23.077713
0.050089	9.207314	0.089083	16.006725	0.121477	23.820201
0.057760	9.570590	0.009023	16 218126	0.122010	23.900812
0.037709	9.474107	0.090102	16.220852	0.122330	24.101740
0.038308	9.376029	0.090702	10.339632	0.123090	24.243008
0.038849	9.082182	0.091242	16.401909	0.125050	24.584590
0.059388	9.786622	0.091782	16.584291	0.1241/6	24.526513
0.059928	9.891348	0.092322	16.707002	0.124/16	24.668/5/
0.060468	9.996363	0.092862	16.830040	0.125256	24.811332
0.061008	10.101661	0.093402	16.953413	0.125796	24.954238
0.061548	10.207246	0.093942	17.077111	0.126335	25.097477
0.062088	10.313114	0.094481	17.201142	0.126875	25.241050
0.062628	10.419265	0.095022	17.325504	0.127415	25.384957
0.063168	10.525698	0.095561	17.450197	0.127955	25.529204
0.063707	10.632414	0.096101	17.575218	0.128495	25.673788
0.064247	10.739413	0.096641	17.700572	0.129035	25.818710
0.064788	10.846694	0.097181	17.826260	0.129575	25.963976
0.065327	10.954256	0.097721	17.952276	0.130115	26.109584
0.065867	11.062101	0.098261	18.078626	0.130655	26.255538
0.066407	11.170224	0.098801	18.205304	0.131195	26.401836
0.066947	11.278631	0.099341	18.332315	0.131735	26.548484
0.067487	11.387319	0.099881	18.459657	0.132274	26.695480
0.068027	11.496287	0.100420	18.587327	0.132814	26.842826
0.068566	11.605540	0.100961	18.715331	0.133354	26.990523
0.069107	11.715073	0.101500	18.843662	0.133894	27.138575
0.069646	11.824890	0.102040	18.972325	0.134434	27.286984
0.070186	11 934990	0 102580	19 101319	0 134974	27 435748
0.070726	12 045374	0.102200	19 230638	0.135514	27.1337.10
0.071266	12.015571	0.103660	19.360287	0.136054	27.301000
0.071806	12.1500 11	0.104200	19.490265	0.136593	27.884188
0.072346	12.200990	0.10/739	19.620572	0.137133	28.03/391
0.072886	12.376240	0.105280	19.020372	0.137673	28.054571
0.072880	12.409709	0.105280	19.751205	0.137073	28.184955
0.0739420	12.001500	0.105319	20.013440	0.138753	28.333879
0.073903	12.713095	0.100333	20.013449	0.130733	20.40/1/1
0.074303	12.820095	0.100899	20.143000	0.139293	20.030023
0.075595	12.938784	0.107439	20.270990	0.139833	28.790847
0.075585	13.051770	0.10/9/9	20.409256	0.1403/3	28.943234
0.076125	13.165050	0.108519	20.541841	0.140912	29.095985
0.076665	13.278624	0.109059	20.674749	0.141453	29.249104
0.077205	13.392497	0.109599	20.807980	0.141993	29.402591
0.077745	13.506667	0.110139	20.941537	0.142532	29.556445
0.078285	13.621139	0.110678	21.075411	0.143072	29.710665
0.078825	13.735912	0.111219	21.209608	0.143612	29.865252
0.079365	13.850985	0.111758	21.344128	0.144152	30.020206
0.079904	13.966366	0.112298	21.478966	0.144692	30.175525
0.080444	14.082053	0.112838	21.614127	0.145232	30.331212
0.080984	14.198045	0.113378	21.749608	0.145772	30.487264
0.081524	14.314344	0.113918	21.885407	0.146312	30.643678
0.082064	14.430956	0.114458	22.021528	0.146851	30.800460
0.082604	14.547877	0.114997	22.157968	0.147392	30.957601

0.147931	31.115108	0.180325	41.185428	0.212719	52.436961
0.148471	31.272974	0.180865	41.363245	0.213259	52.634822
0.149011	31.431200	0.181405	41.541388	0.213798	52.833036
0.149551	31,589785	0.181945	41.719859	0.214339	53.031613
0 150091	31 748727	0 182485	41 898656	0.214878	53 230547
0.150621	21.008027	0.102405	42 077781	0.215418	52 420841
0.150051	31.908027	0.185024	42.077781	0.215418	55.429841
0.1511/0	32.06/681	0.183564	42.257236	0.215958	53.629497
0.151711	32.227690	0.184104	42.437015	0.216498	53.829513
0.152251	32.388050	0.184644	42.617124	0.217038	54.029889
0.152790	32.548759	0.185184	42.797559	0.217578	54.230629
0.153330	32.709821	0.185724	42.978322	0.218118	54.431729
0.153870	32.871226	0.186264	43.159410	0.218658	54.633189
0 154410	33 032980	0 186804	43 340830	0 219198	54 835014
0.15/050	33 105070	0.187344	13.510650	0.219737	55 037100
0.154950	22 257519	0.107344	43.322372	0.219737	55 220742
0.155490	33.337318	0.10/004	43.704043	0.220278	55.239745
0.156030	33.520302	0.188424	43.88/041	0.220817	55.442649
0.156570	33.683424	0.188963	44.069768	0.221357	55.645916
0.157109	33.846888	0.189503	44.252818	0.221897	55.849539
0.157650	34.010685	0.190043	44.436196	0.222437	56.053522
0.158189	34.174821	0.190583	44.619903	0.222977	56.257859
0.158729	34,339290	0.191123	44.803934	0.223517	56.462554
0 159269	34 504093	0 191663	44 988292	0 224057	56 667605
0.150200	24 660220	0.102202	45 172075	0.224037	56 872006
0.159809	34.009229	0.192203	45.172975	0.224397	50.875000
0.160349	34.834696	0.192743	45.35/986	0.225136	5/.0/8/61
0.160889	35.000491	0.193282	45.543320	0.225676	57.284866
0.161428	35.166617	0.193823	45.728985	0.226216	57.491317
0.161969	35.333071	0.194362	45.914972	0.226756	57.698117
0.162508	35.499850	0.194902	46.101288	0.227296	57.905258
0.163048	35.666958	0.195442	46.287933	0.227836	58.112743
0 163589	35 834391	0 195982	46 474902	0 228376	58 320568
0.16/128	36.002150	0.196522	46 662200	0.228916	58 528730
0.164668	26 170222	0.1000522	46.840824	0.220710	58 727220
0.104008	26.229640	0.197002	40.049024	0.229455	50.737229
0.165208	30.338040	0.197602	47.037778	0.229995	58.940001
0.165/48	36.50/3/0	0.198142	47.226060	0.230536	59.155222
0.166288	36.676426	0.198682	47.414671	0.231075	59.364713
0.166828	36.845802	0.199221	47.603610	0.231615	59.574527
0.167367	37.015504	0.199762	47.792882	0.232155	59.784665
0.167908	37.185526	0.200301	47.982483	0.232695	59.995122
0.168447	37.355874	0.200841	48,172417	0.233235	60.205894
0 168987	37 526542	0 201381	48 362684	0 233775	60 41 69 82
0.169527	37 697533	0.201901	48 553282	0.23/315	60 628382
0.100527	27 969940	0.201721	40.555202	0.224855	60.020302
0.170007	20 04049	0.202401	40.744210	0.234833	00.840089
0.170607	38.040480	0.203001	48.935484	0.235394	61.052101
0.171147	38.212446	0.203540	49.12/091	0.235934	61.264417
0.171687	38.384731	0.204081	49.319033	0.236474	61.477033
0.172227	38.557337	0.204620	49.511314	0.237014	61.689943
0.172766	38.730268	0.205160	49.703936	0.237554	61.903146
0.173306	38.903522	0.205700	49.896898	0.238094	62.116641
0 173846	39 077102	0 206240	50 090200	0 238634	62 330425
0 17/386	39 251004	0.206280	50 283846	0.239174	62 544490
0.174026	20 425222	0.200780	50.203040	0.220712	62.544490
0.174920	39.423233	0.207520	50.477859	0.239713	02.738841
0.1/5466	39.399/80	0.207860	50.6/21/6	0.240254	62.9/3468
0.176006	39.774663	0.208400	50.866860	0.240793	63.188371
0.176546	39.949868	0.208940	51.061892	0.241333	63.403549
0.177086	40.125396	0.209479	51.257272	0.241873	63.618995
0.177626	40.301252	0.210020	51.453005	0.242413	63.834711
0.178166	40.477433	0.210559	51.649088	0.242953	64.050690
0.178705	40.653943	0 211099	51,845525	0 243493	64,266931
0 179245	40 830778	0 211630	52 042314	0.244033	64 483/35
0 170785	11 007030	0.212170	57 720/61	0.244033	64 700104
V.1/7/0.)	+1.00/737	0.2121/9	JZ.ZJ7401	(1,2+4,1,1,1)	04./00194

0 245113	64 017207	0 277506	78 370826	0.300000	02 606578
0.245115	04.917207	0.277300	78.570820	0.309900	92.090378
0.245652	65.134473	0.278046	/8.602668	0.310440	92.940723
0.246193	65.351990	0.278586	78.834783	0.310980	93.185007
0.246732	65.569754	0.279126	79.067174	0.311520	93.429434
0.247272	65.787763	0.279666	79.299841	0.312060	93.674007
0.247812	66.006018	0.280206	79.532780	0.312599	93.918727
0 248352	66 224512	0 280746	79 765996	0 313140	94 163597
0.248802	66 443248	0.281286	79 999/8/	0.313670	94 408616
0.240092	66 662220	0.281280	20 022045	0.313079	94.408010
0.249432	00.002220	0.281825	80.233245	0.314219	94.055/91
0.249971	66.881428	0.282365	80.46/280	0.314/59	94.899123
0.250512	67.100870	0.282905	80.701582	0.315299	95.144615
0.251051	67.320545	0.283445	80.936155	0.315839	95.390267
0.251591	67.540455	0.283985	81.170995	0.316379	95.636088
0.252131	67.760592	0.284525	81.406101	0.316919	95.882079
0.252671	67.980961	0.285065	81.641472	0.317459	96.128240
0.253211	68 201555	0.285605	81 877102	0 317998	96 374578
0.253211	68 422378	0.286144	82 112003	0.318538	06 621006
0.253751	68 6 42 4 27	0.280144	82.112333	0.310330	90.021090
0.254291	68.643427	0.286685	82.349141	0.319078	96.86/801
0.254831	68.864702	0.287225	82.585541	0.319618	97.114690
0.255371	69.086202	0.287764	82.822193	0.320158	97.361776
0.255910	69.307928	0.288304	83.059095	0.320698	97.609054
0.256451	69.529877	0.288844	83.296238	0.321238	97.856533
0.256990	69.752052	0.289384	83.533625	0.321778	98.104218
0 257530	69 974451	0 289924	83 771248	0 322318	98 352112
0.258070	70 197075	0 290464	84 009105	0.322858	98 600217
0.258610	70.410022	0.201004	84 247104	0.322050	08 848542
0.250150	70.419922	0.291004	04.247174	0.323398	90.040J42
0.259150	70.642997	0.291544	84.485508	0.323937	99.097085
0.259690	/0.866296	0.292083	84.724045	0.324477	99.345856
0.260229	71.089823	0.292624	84.962803	0.325017	99.594856
0.260770	71.313576	0.293163	85.201773	0.325557	99.844089
0.261309	71.537558	0.293703	85.440953	0.326097	100.093562
0.261849	71.761770	0.294243	85.680341	0.326637	100.343276
0.262389	71.986211	0.294783	85.919931	0.327177	100.593239
0.262929	72 210886	0.295323	86 159721	0 327717	100 843449
0.262/29	72.435791	0.295863	86 300702	0.328256	101.003017
0.203409	72.433791	0.295805	86.620875	0.328230	101.093917
0.264009	72.000933	0.290402	80.039873	0.328790	101.544041
0.264549	/2.886311	0.296943	86.880234	0.329336	101.595631
0.265089	73.111926	0.297482	87.120775	0.329876	101.846884
0.265629	73.337779	0.298022	87.361493	0.330416	102.098409
0.266168	73.563874	0.298562	87.602388	0.330956	102.350210
0.266709	73.790213	0.299102	87.843451	0.331496	102.602287
0.267248	74.016796	0.299642	88.084685	0.332036	102.854648
0.267788	74.243626	0.300182	88.326079	0.332575	103.107292
0.268328	74 470706	0.300722	88 567638	0.333116	103 360227
0.268868	74.608035	0.301262	88 800352	0.333656	103.500227
0.208808	74.036033	0.301202	88.809332	0.333030	102.013434
0.269408	74.925018	0.301802	89.051221	0.334195	103.800980
0.269948	/5.153454	0.302341	89.293242	0.334/35	104.120806
0.270488	75.381547	0.302882	89.535413	0.335275	104.374936
0.271028	75.609897	0.303421	89.777733	0.335815	104.629373
0.271567	75.838507	0.303961	90.020198	0.336355	104.884125
0.272107	76.067380	0.304501	90.262805	0.336895	105.139190
0.272647	76.296515	0.305041	90.505556	0.337435	105.394575
0 273187	76 525916	0 305581	90 748446	0 337975	105 650283
0 273727	76 755584	0 306121	90 991/178	0.338514	105 006300
0.273727	76 095520	0.206660	01 224640	0.220055	105.900322
0.274207	10.703320	0.300000	71.234049 01.477057	0.339033	100.102088
0.2/480/	//.215/24	0.307201	91.4//95/	0.339394	106.419391
0.275347	//.446198	0.307740	91.721404	0.340134	106.676436
0.275887	77.676946	0.308280	91.964990	0.340674	106.933827
0.276426	77.907966	0.308820	92.208715	0.341214	107.191564
0.276967	78.139259	0.309360	92.452577	0.341754	107.449656

0.342294	107.708108	0.374687	124.324727	0.407081	149.357246
0.342833	107.966924	0.375227	124.635510	0.407620	149.904335
0.343374	108.226108	0.375767	124.948341	0.408161	150.453679
0 343913	108 485671	0 376307	125 263309	0 408700	151 004819
0.344453	108 745611	0.376847	125.200009	0.409240	151.557/21
0.344003	100.745011	0.370047	125.500450	0.400240	152 111252
0.344993	109.003940	0.377387	125.899998	0.409780	152.111252
0.345533	109.266662	0.377927	126.221905	0.410320	152.666159
0.346073	109.527784	0.378467	126.546314	0.410860	153.221982
0.346613	109.789315	0.379006	126.873328	0.411400	153.778499
0.347153	110.051259	0.379547	127.203052	0.411940	154.335360
0.347693	110.313628	0.380086	127.535590	0.412480	154.892060
0.348233	110.576424	0.380626	127.871045	0.413019	155.447965
0.348772	110.839660	0.381166	128.209524	0.413559	156.002332
0 349313	111 103344	0 381706	128 551120	0 414099	156 554388
0.349852	111 367488	0.382246	128 895924	0.414639	157 103375
0.347032	111.507400	0.302240	120.073724	0.415170	157 649504
0.350392	111.052090	0.362760	129.244016	0.415179	157.040394
0.350932	111.89/180	0.383325	129.5954/3	0.415/19	158.189389
0.351472	112.162754	0.383866	129.950349	0.416259	158.725125
0.352012	112.428828	0.384405	130.308695	0.416799	159.255116
0.352552	112.695413	0.384945	130.670568	0.417339	159.778612
0.353091	112.962521	0.385485	131.036024	0.417879	160.294770
0.353632	113.230167	0.386025	131.405136	0.418419	160.802675
0.354171	113.498362	0.386565	131.777993	0.418958	161.301397
0 354711	113 767124	0 387105	132 154711	0 419498	161 789995
0.355251	11/ 036/66	0.387645	132 535/32	0.420038	162 267565
0.355701	114.000400	0.307045	122.000200	0.420030	162.207303
0.353791	114.500404	0.300103	132.320303	0.420378	162.195221
0.356331	114.5/6954	0.388724	133.309518	0.421118	163.186096
0.3568/1	114.848137	0.389264	133.703228	0.421658	163.625319
0.357411	115.119968	0.389804	134.101595	0.422198	164.050001
0.357951	115.392466	0.390344	134.504748	0.422738	164.459251
0.358491	115.665654	0.390884	134.912775	0.423277	164.852157
0.359030	115.939552	0.391424	135.325719	0.423818	165.227801
0.359571	116.214179	0.391964	135.743572	0.424357	165.585244
0.360110	116.489562	0.392504	136.166283	0.424897	165.923532
0.360650	116 765726	0 393043	136 593762	0 425437	166 241685
0.361190	117 0/2692	0.393584	137 025903	0.425977	166 538731
0.361720	117.042072	0.375504	127 462610	0.426517	166 912719
0.301730	117.520460	0.394123	137.402010	0.420317	100.015/10
0.362270	117.599141	0.394003	137.903807	0.427057	167.065727
0.362810	11/.8/86/8	0.395203	138.349481	0.42/596	167.293909
0.363350	118.159128	0.395743	138.799699	0.428137	167.497485
0.363890	118.440524	0.396283	139.254606	0.428676	167.675751
0.364429	118.722897	0.396823	139.714415	0.429216	167.828075
0.364969	119.006275	0.397363	140.179367	0.429756	167.953891
0.365509	119.290695	0.397903	140.649694	0.430296	168.052681
0.366049	119.576192	0.398443	141.125548	0.430836	168.123948
0 366589	119 862800	0 398982	141 606954	0 431375	168 167197
0.367129	120 150554	0.399522	142 093798	0.431916	168 181911
0.367660	120.130354	0.377322	142.075770	0.432456	168 167513
0.307009	120.439490	0.400002	142.303027	0.432430	100.107313
0.368209	120.729001	0.400602	143.082082	0.432995	108.123441
0.368/48	121.021097	0.401142	143.583969	0.433535	168.049118
0.369289	121.313842	0.401682	144.089330	0.434075	167.943996
0.369828	121.607943	0.402222	144.598512	0.434615	167.807601
0.370368	121.903448	0.402762	145.111393	0.435155	167.639572
0.370908	122.200411	0.403301	145.628005	0.435694	167.439653
0.371448	122.498878	0.403842	146.148492	0.436235	167.207698
0.371988	122,798909	0.404381	146.673043	0.436774	166.943649
0 372528	123 100566	0 404921	147 201816	0 437314	166 647500
0 373068	123 /03006	0.107921	147 73/8/2	0 / 27 85/	166 310302
0.373608	123.403200	0.405401	1/8 271004	0.437034	165 050124
0.373000	123.709002	0.400001	140.2/1990 140.010051	0.430374	105.757154
U. 7/4148	124.010918	0.400541	140.012921	0.4.58954	10.3.30/118

0.439474	165.143399	0.471867	106.230516	0.504261	64.336940
0.440014	164.688124	0.472407	105.268979	0.504801	63.842774
0.440554	164.201432	0.472947	104.319769	0.505341	63.353853
0.441093	163.683411	0.473487	103.382691	0.505880	62.870139
0.441633	163.134111	0.474027	102.457462	0.506420	62.391607
0 442173	162 553579	0 474567	101 543751	0.506960	61 918232
0.442713	161 9/1911	0.475107	100.6/1223	0.507500	61 // 9993
0.442713	161 200323	0.475646	00 740570	0.507500	60.086873
0.443233	160 626107	0.475196	00 060500	0.508590	60.528952
0.443793	150.022101	0.470180	07.008042	0.508580	60.075010
0.444333	159.925101	0.470720	97.990042	0.509120	50 628051
0.444873	159.190744	0.477200	97.157810	0.309000	59.028051
0.445413	158.429922	0.4778246	96.287768	0.510199	59.185237
0.445952	15/.04143/	0.478346	95.447758	0.510/40	58.747453
0.446493	156.826054	0.4/8886	94.61/635	0.511279	58.314684
0.447032	155.984471	0.479426	93.797235	0.511819	57.886906
0.447572	155.117339	0.479965	92.986391	0.512359	57.464090
0.448112	154.225309	0.480506	92.184954	0.512899	57.046210
0.448652	153.309070	0.481045	91.392778	0.513439	56.633232
0.449192	152.369375	0.481585	90.609746	0.513979	56.225119
0.449732	151.407037	0.482125	89.835741	0.514519	55.821829
0.450272	150.422926	0.482665	89.070649	0.515059	55.423323
0.450812	149.417948	0.483205	88.314332	0.515599	55.029551
0.451351	148.393037	0.483745	87.566634	0.516138	54.640472
0.451891	147.349180	0.484284	86.827364	0.516678	54.256039
0.452431	146.287425	0.484825	86.096310	0.517218	53.876208
0.452971	145.208928	0.485364	85.373239	0.517758	53.500940
0.453511	144.114937	0.485904	84.657922	0.518298	53.130190
0.454051	143.006797	0.486444	83.950152	0.518838	52.763923
0 454591	141 885914	0 486984	83 249766	0 519378	52 402100
0.455131	140 753703	0.487524	82 556642	0.519918	52.044685
0.455670	139 611551	0 488064	81 870725	0.520457	51 691642
0.456211	138 460791	0.488604	81 191999	0.520197	51 342942
0.456750	137 302691	0.480144	80 520/80	0.520590	50 998544
0.457290	136 138/68	0.489684	70 856180	0.521557	50 658/10
0.457830	134.060302	0.400223	79.000109	0.522617	50 222522
0.457850	134.909302	0.490223	79.199134	0.522017	40 000851
0.436570	133.790302	0.490704	70.349200	0.525157	49.990631
0.458910	132.020820	0.491303	77.900577	0.523097	49.003330
0.459450	131.443870	0.491843	77.270880	0.524257	49.339950
0.459989	130.200090	0.492383	76.642073	0.524776	49.020658
0.460530	129.090476	0.492923	/6.019964	0.525317	48./05419
0.461069	127.916432	0.493463	75.404381	0.525856	48.394193
0.461609	126.745732	0.494003	74.795157	0.526396	48.086933
0.462149	125.579534	0.494543	74.192138	0.526936	47.783596
0.462689	124.418950	0.495083	73.595191	0.527476	47.484131
0.463229	123.265006	0.495622	73.004212	0.528016	47.188495
0.463769	122.118642	0.496162	72.419122	0.528556	46.896631
0.464309	120.980698	0.496702	71.839874	0.529096	46.608488
0.464849	119.851930	0.497242	71.266443	0.529636	46.324015
0.465389	118.733044	0.497782	70.698823	0.530176	46.043155
0.465928	117.624710	0.498322	70.137019	0.530715	45.765852
0.466469	116.527556	0.498862	69.581048	0.531256	45.492052
0.467008	115.442138	0.499402	69.030917	0.531795	45.221696
0.467548	114.368883	0.499941	68.486624	0.532335	44.954733
0.468088	113.308060	0.500481	67.948150	0.532875	44.691103
0.468628	112.259761	0.501021	67.415457	0.533415	44.430756
0.469168	111.223965	0.501561	66.888490	0.533955	44.173631
0.469708	110.200579	0.502101	66.367182	0.534495	43.919679
0.470247	109.189536	0.502641	65.851449	0.535035	43.668844
0.470788	108.190819	0.503181	65.341215	0.535575	43.421078
0.471327	107.204463	0.503721	64.836402	0.536114	43,176324

0.536654	42.934534	0.561490	34.276139	0.779599	19.453705
0.537194	42.695658	0.562029	34.129016	0.784612	19.347055
0.537734	42.459646	0.562569	33.983277	0.789626	19.242749
0.538274	42.226449	0.563109	33.838904	0.794639	19.140790
0.538814	41.996020	0.563649	33.695882	0.799653	19.041158
0.539354	41.768310	0.564189	33.554200	0.804667	18.943841
0.539894	41.543273	0.564729	33.413843	0.809680	18.848814
0.540433	41.320862	0.565269	33.274799	0.814694	18.756055
0.540974	41.101029	0.565808	33.137100	0.819707	18.665530
0.541513	40.883732	0.574164	31.162902	0.824721	18.577214
0.542053	40.668924	0.582520	29.465950	0.829734	18.491068
0.542593	40.456563	0.590876	28.014568	0.834747	18.407065
0.543133	40.246599	0.599232	26.795590	0.839760	18.325173
0.543673	40.038993	0.607587	25.790273	0.844773	18.245369
0.544213	39.833703	0.615938	24.982746	0.849785	18.167654
0.544753	39.630686	0.624280	24.348118	0.854796	18.091982
0.545293	39.429898	0.629283	24.037303	0.859805	18.018541
0.545833	39.231300	0.634289	23.769494	0.864811	17.947031
0.546372	39.034852	0.639294	23.533619	0.869813	17.878292
0.546912	38.840518	0.644301	23.320707	0.874812	17.810465
0.547452	38.648258	0.649309	23.123346	0.879816	17.741572
0.547992	38.458033	0.654319	22.936557	0.884826	17.677444
0.548532	38.269808	0.659331	22.757291	0.889837	17.613201
0.549072	38.083550	0.664343	22.583805	0.894848	17.551657
0.549612	37.899224	0.669356	22.415093	0.899857	17.491614
0.550152	37.716796	0.674369	22.250543	0.904861	17.433346
0.550691	37.536233	0.679382	22.089757	0.909868	17.375034
0.551232	37.357507	0.684395	21.932461	0.914877	17.319082
0.551771	37.180585	0.689409	21.778454	0.919889	17.262886
0.552311	37.005441	0.694421	21.627614	0.924899	17.208937
0.552851	36.832047	0.699433	21.480014	0.929907	17.155792
0.553391	36.660371	0.704439	21.335889	0.934913	17.103709
0.553931	36.490394	0.709441	21.196693	0.939913	17.053119
0.554471	36.322086	0.714442	21.057432	0.944920	16.999926
0.555010	36.155424	0.719445	20.920501	0.949924	16.949346
0.555551	35.990386	0.724455	20.783067	0.954935	16.897589
0.556090	35.826948	0.729466	20.649773	0.959945	16.847923
0.556630	35.665089	0.734478	20.519280	0.964951	16.798519
0.557171	35.504786	0.739491	20.391400	0.969960	16.749406
0.557710	35.346022	0.744504	20.265969	0.974968	16.701882
0.558250	35.188776	0.749517	20.142904	0.979978	16.655056
0.558790	35.033026	0.754531	20.022189	0.984982	16.611192
0.559330	34.878759	0.759544	19.903808	0.989989	16.567929
0.559870	34.725953	0.764558	19.787766	0.994993	16.527578
0.560410	34.574593	0.769571	19.674063	1.000000	16.488471
0.560949	34.424661	0.774585	19.562711		

Step 2: INT1 \rightarrow TS2 \rightarrow INT2 + H₂O

		0.025728	0.293838	0.072893	1.271157
Intrinsic	Electronic	0.030017	0.358966	0.077179	1.393395
Coordinate	Energy	0.034305	0.425932	0.081465	1.527203
	(kJ/mol)	0.038594	0.499987	0.085747	1.662900
		0.042878	0.576140	0.090034	1.807728
0.000000	0.000000	0.047166	0.656527	0.094325	1.960364
0.004288	0.039490	0.051458	0.746669	0.098616	2.124988
0.008573	0.081666	0.055746	0.838522	0.102904	2.294556
0.012864	0.129461	0.060034	0.939929	0.107187	2.473021
0.017151	0.179734	0.064316	1.042208	0.111465	2.661173
0.021442	0.236032	0.068602	1.151001	0.115738	2.861813

0 120021	3 064494	0 238064	13 211120	0 263500	17 847298
0.124310	3 28/858	0.238488	13 268067	0.263924	17.060565
0.124510	3 511013	0.230400	13.200007	0.263324	18.075706
0.120097	2.751055	0.236912	12 292245	0.204343	18.073790
0.132887	3.751955	0.239335	13.383245	0.264773	18.193043
0.13/1/2	3.997770	0.239759	13.441486	0.265197	18.312358
0.141462	4.261150	0.240184	13.500171	0.265620	18.433796
0.145749	4.530878	0.240608	13.559305	0.266044	18.557412
0.150037	4.816614	0.241032	13.618896	0.266468	18.683260
0.154318	5.105377	0.241456	13.678952	0.266892	18.811398
0.158605	5.408992	0.241880	13.739483	0.267317	18.941877
0.162881	5.723359	0.242303	13.800494	0.267741	19.074762
0 167166	6 049924	0 242727	13 861994	0 268165	19 210109
0.171444	6 385912	0.243152	13 973998	0.268588	19.210105
0.175716	6 733116	0.243132	13.025550	0.260012	10 / 88 / 20
0.175710	7.002127	0.243370	13.300311	0.209012	19.400420
0.100000	7.093127	0.244000	14.049347	0.209450	19.031307
0.184298	7.464247	0.244424	14.113115	0.269860	19.///301
0.188591	7.849111	0.244848	14.177230	0.270285	19.925862
0.192884	8.246076	0.245272	14.241901	0.270709	20.077259
0.197177	8.656087	0.245695	14.307145	0.271133	20.231552
0.201471	9.079475	0.246120	14.372972	0.271557	20.388811
0.205764	9.517338	0.246544	14.439399	0.271980	20.549106
0.210057	9.970494	0.246968	14.506441	0.272404	20.712504
0.214349	10.440865	0.247392	14.574111	0.272828	20.879073
0 218640	10 922868	0.247816	14 642432	0 273253	21 048888
0.222800	11 461707	0.248240	14 711414	0.273677	21.010000
0.222000	11.401/07	0.248663	14.791097	0.273077	21.222017
0.223224	11.499030	0.248003	14./0100/	0.274101	21.376337
0.223048	11.55/941	0.249088	14.801408	0.274525	21.578522
0.224072	11.577350	0.249512	14.922594	0.274948	21.762050
0.224495	11.617767	0.249935	14.994425	0.275372	21.949193
0.224919	11.659100	0.250359	15.067193	0.275796	22.140033
0.225343	11.701271	0.250783	15.140434	0.276221	22.334645
0.225768	11.744213	0.251206	15.214788	0.276645	22.533112
0.226192	11.787873	0.251630	15.289350	0.277069	22.735515
0.226615	11.832202	0.252053	15.365088	0.277493	22.941931
0.227039	11.877161	0.252477	15.441505	0.277916	23.152447
0.227463	11.922713	0.252901	15.519015	0.278340	23.367139
0 227887	11 968833	0 253325	15 597463	0 278765	23 586095
0.228311	12 015493	0 253749	15 676921	0 279189	23 809391
0.228736	12.013 193	0.254172	15 757377	0.279613	24.037112
0.220750	12.002071	0.254506	15 939962	0.279013	24.037112
0.229100	12.110347	0.254590	15.030002	0.280037	24.209340
0.229383	12.138307	0.233020	15.921397	0.280401	24.306134
0.230007	12.20/136	0.255444	16.005011	0.280884	24.747637
0.230431	12.256220	0.255869	16.089/36	0.281308	24.993870
0.230855	12.305747	0.256292	16.175606	0.281733	25.244931
0.231279	12.355711	0.256716	16.262652	0.282157	25.500896
0.231704	12.406104	0.257140	16.350913	0.282581	25.761847
0.232128	12.456918	0.257564	16.440419	0.283005	26.027857
0.232552	12.508150	0.257988	16.531214	0.283429	26.299006
0.232975	12.559791	0.258412	16.623332	0.283853	26.575361
0.233399	12.611841	0.258837	16.716816	0.284276	26.856996
0.233823	12.664299	0.259261	16.811701	0.284701	27.143981
0 234247	12 717158	0 259684	16 908031	0.285125	27 436388
0 234672	12.770421	0.260108	17 005849	0 285549	27 734278
0.235006	12.770 121	0.260532	17 105108	0.285072	28 027717
0.235070	12.024007	0.200332	17.105190	0.205915	20.03//1/
0.233320	12.070130	0.200930	17.20011/	0.20037/	20.340/0/
0.233943	12.932028	0.201380	17.308033	0.280821	28.001489
0.236367	12.98/506	0.261805	1/.41285/	0.28/244	28.981936
0.236791	13.042791	0.262229	17.518775	0.287669	29.308170
0.237215	13.098486	0.262652	17.626454	0.288093	29.640236
0.237640	13.154595	0.263076	17.735946	0.288517	29.978190

0.000011	20 222075	0.01.4001	60 (E 100E	0.000001	100 110010
0.288941	30.322075	0.314381	62.654005	0.339821	123.418813
0.289365	30.671939	0.314805	63.396772	0.340245	124.802722
0.289789	31.027823	0.315229	64.146746	0.340669	126.199102
0.290213	31 389772	0 315653	64 903943	0 341094	127 607644
0.200627	21 757917	0.316077	65 669290	0.241518	120.027061
0.290037	31./3/81/	0.310077	03.008389	0.341318	129.027901
0.291061	32.132001	0.316501	66.440105	0.341942	130.459486
0.291485	32.512352	0.316925	67.219130	0.342366	131.901402
0.291909	32.898907	0.317349	68.005494	0.342789	133.352668
0.292333	33.291692	0.317773	68.799245	0.343213	134.812063
0 292757	33 690736	0 318197	69 600443	0 343637	136 278237
0.202191	34,006066	0.218621	70 400160	0.344062	127 740767
0.293161	34.090000	0.316021	70.409100	0.344002	137.749707
0.293605	34.507705	0.319045	71.225499	0.344486	139.225219
0.294029	34.925677	0.319469	72.049591	0.344910	140.703189
0.294453	35.350000	0.319893	72.881591	0.345334	142.182330
0.294877	35.780695	0.320317	73.721664	0.345757	143.661371
0 295301	36 217780	0 320741	74 569981	0 346181	145 139087
0.205725	26 661272	0.320741	75 426602	0.346606	146 614261
0.293723	30.001272	0.321103	75.420095	0.340000	140.014201
0.296149	37.111185	0.321589	76.291913	0.34/030	148.085649
0.296573	37.567531	0.322013	77.165721	0.347454	149.551977
0.296997	38.030320	0.322437	78.048162	0.347878	151.011928
0.297421	38.499565	0.322861	78.939257	0.348302	152.464169
0 297845	38 975274	0.323285	79.839016	0 348726	153 907338
0.207045	20 457452	0.323203	P0.747462	0.340120	155 240069
0.298209	39.437433	0.525710	80.747405	0.549149	155.540008
0.298693	39.946106	0.324133	81.664636	0.349574	156.760954
0.299117	40.441241	0.324557	82.590603	0.349998	158.168564
0.299541	40.942858	0.324981	83.525454	0.350422	159.561410
0.299965	41.450969	0.325405	84.469319	0.350846	160.937959
0.300389	41 965572	0.325829	85 422367	0 351270	162 296648
0.200912	42 486670	0.226252	96 294910	0.351270	162.220040
0.500815	42.480079	0.520255	80.384810	0.551094	105.055907
0.301237	43.014291	0.326678	87.356904	0.352118	164.954210
0.301661	43.548423	0.327102	88.338933	0.352542	166.250128
0.302085	44.089082	0.327525	89.331183	0.352966	167.522385
0.302509	44.636278	0.327949	90.333919	0.353390	168.769886
0.302933	45 190019	0 328373	91 347357	0 353814	169 991741
0.302355	45 750322	0.328707	02 371641	0.354238	171 187252
0.303337	45.750522	0.326797	92.371041	0.334238	171.107232
0.303/81	46.31/196	0.329221	93.406852	0.354662	1/2.355862
0.304205	46.890648	0.329646	94.453024	0.355086	173.497065
0.304629	47.470689	0.330070	95.510171	0.355510	174.610324
0.305053	48.057328	0.330493	96.578327	0.355934	175.694976
0.305477	48.650578	0.330917	97.657597	0.356358	176.750204
0.305901	49 250442	0 331341	98 7/8177	0 356782	177 775026
0.305701	40.956022	0.221765	00.950400	0.350702	179.769247
0.500525	49.830932	0.551/05	99.830409	0.557200	170.700347
0.306/49	50.470055	0.332190	100.964739	0.357630	179.729023
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0.307597	51.716230	0.333038	103.231903	0.358478	181.548066
0.308021	52.349288	0.333462	104.385784	0.358902	182.404520
0 308445	52 988994	0 333885	105 553696	0 359326	183 224613
0.308960	52 625250	0.3333005	106 725782	0.3597520	103.221013
0.308809	53.055552	0.334309	100.755785	0.339730	104.007671
0.309293	54.288364	0.334/33	107.932010	0.360174	184./54043
0.309717	54.948031	0.335158	109.142253	0.360598	185.463080
0.310141	55.614368	0.335582	110.366416	0.361022	186.135093
0.310565	56.287396	0.336006	111.604560	0.361446	186.770291
0 310989	56 967149	0 336429	112 856955	0 361870	187 368905
0 311/12	57 653672	0 336853	11/ 12/050	0 362204	187 031110
0.311413	51.033012	0.330033	114.124030	0.302274	107.731119
0.31183/	58.547022	0.337277	115.400550	0.362/18	188.45/01/
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0.313533	61.189995	0.338974	120.690079	0.364414	190.194037
0.212057	61 918/21	0 339397	122 047754	0 36/838	190 53/990

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0.366110	191.330763	0.391550	166.670978	0.416990	134.109863
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0 366958	191 674977	0 392398	165 469583	0 417838	133 151327
0.367382	191.07 1977	0.392822	16/ 872132	0.117050	132 67/888
0.367806	101 876536	0.302022	164 276700	0.418686	132.074000
0.307800	191.070330	0.393240	164.270700	0.410000	132.200329
0.368230	191.925988	0.393070	163.083007	0.419110	131.727044
0.368654	191.942331	0.394094	163.090985	0.419534	131.256821
0.369078	191.926282	0.394518	162.500250	0.419958	130.787854
0.369502	191.878500	0.394942	161.910739	0.420383	130.320723
0.369926	191.799565	0.395366	161.322435	0.420806	129.855416
0.370350	191.690021	0.395790	160.735420	0.421230	129.391907
0.370774	191.550431	0.396214	160.149876	0.421654	128.930176
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0.372046	190.958097	0.397486	158.404404	0.422926	127.555410
0.372470	190.705616	0.397910	157.827028	0.423351	127,100544
0.372894	190.427336	0.398334	157.252109	0.423775	126.647333
0 373318	190 124438	0 398758	156 679685	0 424198	126 195752
0.373742	180 7081/3	0.300182	156 100731	0.121190	125.745784
0.373742	189.790145	0.399102	155 542181	0.424022	125.745784
0.374100	109.449003	0.399000	153.542101	0.425040	123.297403
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0.375014	188.690718	0.400454	154.413933	0.425894	124.405342
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0.375862	187.855951	0.401302	153.294270	0.426743	123.519446
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0.378830	184.451441	0.404270	149.440735	0.429711	120.465966
0.379254	183.917241	0.404694	148.898845	0.430135	120.035597
0.379678	183.373545	0.405118	148.359202	0.430559	119.606658
0.380102	182.821045	0.405542	147.821820	0.430982	119.179138
0.380526	182.260527	0.405966	147.286696	0.431406	118,753027
0.380950	181.692883	0.406390	146.753816	0.431831	118.328313
0 381374	181 119065	0 406814	146 223153	0 432255	117 904988
0 381798	180 539998	0 407238	145 694684	0.432679	117 483041
0.382222	179 956470	0.107250	1/15 168382	0.132079	117.062465
0.382646	170 360050	0.407002	144 644222	0.433527	116 643240
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0.383070	170.770124	0.408024	144.122191	0.433931	115 200265
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0.384/66	1/6.382461	0.410206	142.055164	0.435647	114.56/331
0.385190	175.776899	0.410630	141.543648	0.436071	114.156149
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0.386462	173.953411	0.411902	140.021478	0.437343	112.930563
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0.388582	170.916471	0.414022	137.524546	0.439463	110.914563
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0.389430	169.701807	0.414870	136.539377	0.440311	110.117576
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0.442007	108.339900	0.407443	87.232312	0.492880	09.874393
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0.443279	107.371211	0.468718	86.292091	0.494158	69.094509
0.443703	106.984394	0.469142	85.974368	0.494582	68.836323
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0 444551	106 214910	0 469989	85 342473	0 495430	68 322743
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0.445200	105.052250	0.470929	84 715202	0.406278	67.812020
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0.447943	103.191707	0.473381	82.862229	0.498822	66.306417
0.448367	102.819834	0.473806	82.557461	0.499246	66.058712
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0.449639	101./11954	0.4/50/8	81.649991	0.500518	05.521415
0.450063	101.345193	0.475502	81.349742	0.500942	65.077583
0.450487	100.979673	0.475926	81.050595	0.501366	64.834719
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0.452607	99 170257	0.478046	79 570931	0 503486	63 634713
0.452007	98 812021	0.478470	79.278125	0.503400	63 30753/
0.452455	90.012021	0.478904	79.276125	0.503910	62 161079
0.455455	98.433403	0.478894	78.980330	0.304334	03.101278
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0.454302	97.746289	0.479742	78.405724	0.505182	62.691505
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0.455573	96.686469	0.481014	77.542118	0.506454	61.993553
0.455997	96.335571	0.481438	77.256157	0.506879	61.762653
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0.459813	93.223886	0.485254	74.723802	0.510694	59.722254
0.460237	92.883201	0.485678	74.446914	0.511118	59.499598
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0.461085	92 204866	0.486526	73 895787	0.511966	59.056653
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0.461024	01 520610	0.480950	73.021343	0.512590	59 616945
0.401954	91.330019	0.467374	73.348170	0.512815	50.010045
0.462358	91.195044	0.487798	/3.0/5689	0.513239	58.398109
0.462781	90.860510	0.488222	72.804075	0.513663	58.180153
0.463205	90.527030	0.488646	72.533339	0.514086	57.962969
0.463629	90.194613	0.489070	72.263482	0.514510	57.746562
0.464053	89.863264	0.489494	71.994502	0.514934	57.530927
0.464477	89.533000	0.489918	71.726402	0.515359	57.316064
0.464902	89.203828	0.490342	71.459187	0.515783	57.101971
0.465326	88 875758	0 490766	71 192856	0 516207	56 8886/10
0.465750	88 5/8802	0/01100	70 927/13	0.516631	56 676004
0.466172	88 222070	0.401614	70.662862	0.517055	56 161205
0.4001/3	00.222770	0.471014	70.002002	0.517055	50.404505
0.40059/	01.090212	0.4920.58	/0.599204	0.51/4/8	50.255280

0.517902	56.043015	0.543343	44.696591	0.631818	19.300392
0.518327	55.833510	0.543767	44.528047	0.639246	17.775575
0.518751	55.624759	0.544191	44.360138	0.646674	16.306482
0.519175	55.416759	0.544615	44.192860	0.654102	14.899048
0 519599	55 209508	0 545039	44 026209	0.661452	13 564858
0.520023	55 002999	0 545463	43 860180	0.668802	12 277198
0.520025	54 707225	0.545887	43.60/773	0.676154	11.031768
0.520447	54.797223	0.545007	43.074773	0.692505	0.820122
0.520870	54.392182	0.540511	43.329984	0.085505	9.850152
0.521295	54.38/868	0.546735	43.365811	0.690856	8.664218
0.521719	54.184271	0.547159	43.202256	0.698207	7.533720
0.522143	53.981388	0.547583	43.039317	0.705558	6.441677
0.522567	53.779214	0.548007	42.876993	0.712909	5.388277
0.522991	53.577738	0.548431	42.715283	0.717262	4.781036
0.523415	53.376961	0.548855	42.554193	0.721615	4.184519
0.523839	53.176869	0.549279	42.393728	0.725969	3.598145
0.524263	52.977462	0.549703	42.233885	0.730322	3.024421
0.524687	52.778733	0.550127	42.074711	0.734676	2.462974
0.525111	52,580673	0.550551	41,916139	0.739030	1.912251
0 525535	52 383283	0 550975	41 758352	0 743383	1 371131
0.525959	52 186557	0 551399	41 600956	0 747737	0.840937
0.526383	51 000/00	0.551822	41.000990	0.747797	0.322327
0.526807	51 705070	0.552246	41.444.504	0.752091	0.322327
0.520807	51.795079	0.552240	41.200077	0.750444	-0.163630
0.527251	51.000525	0.552070	41.132330	0.760793	-0.077823
0.527655	51.406221	0.553094	40.977504	0.765140	-1.156155
0.528079	51.212/69	0.553518	40.823135	0.769488	-1.635868
0.528503	51.019968	0.553942	40.669363	0.773838	-2.097861
0.528927	50.827821	0.554366	40.516201	0.778191	-2.558240
0.529351	50.636325	0.554790	40.363639	0.782544	-3.004614
0.529775	50.445480	0.555214	40.211670	0.786897	-3.443010
0.530199	50.255294	0.555638	40.060291	0.791248	-3.870391
0.530623	50.065767	0.556062	39.909493	0.795599	-4.288528
0.531047	49.876899	0.556486	39.759275	0.799946	-4.694953
0.531471	49.688695	0.556910	39.609624	0.804293	-5.091884
0.531895	49.501159	0.557334	39.460538	0.808636	-5.480440
0.532319	49.314294	0.557758	39.312008	0.812982	-5.863327
0.532743	49.128104	0.558182	39.164024	0.817329	-6.240617
0.533167	48.942591	0.558607	39.016581	0.821679	-6.609040
0 533591	48 757759	0 559030	38 869669	0.826029	-6 968298
0.534015	48 573614	0 559454	38 723282	0.830381	-7 318589
0.534439	48.390155	0.559878	38 577404	0.834733	-7 660385
0.524962	40.370133	0.560202	29 422022	0.034735	7.004267
0.534805	40.207300	0.500302	20 207157	0.839085	-7.334207
0.555267	40.023313	0.500720	20.20/13/	0.043430	-0.520590
0.555711	47.643933	0.501150	56.142706 27.000056	0.847784	-8.039129
0.536135	47.663246	0.561575	37.998856	0.852130	-8.950135
0.536559	47.483260	0.561999	37.855415	0.856478	-9.260973
0.536983	47.303967	0.562422	37.712430	0.860829	-9.559858
0.537407	47.125370	0.562846	37.569899	0.865181	-9.856747
0.537831	46.947471	0.563270	37.427813	0.869532	-10.144184
0.538255	46.770263	0.563694	37.286162	0.873881	-10.424844
0.538679	46.593748	0.564118	37.144941	0.878232	-10.703058
0.539103	46.417918	0.564543	37.004144	0.882579	-10.972303
0.539527	46.242777	0.564967	36.863779	0.886929	-11.238986
0.539951	46.068315	0.572395	34.469163	0.891278	-11.499511
0.540375	45.894530	0.579823	32.200655	0.895627	-11.754316
0.540799	45.721418	0.587251	30.053747	0.899977	-12.005823
0 541223	45 548972	0 594679	28 013859	0.904328	-12 252308
0 541647	45 377191	0.602107	26.086193	0.909520	-12.252500
0.542071	45 206066	0.600534	20.000175	0.013074	12.792040
0.542071	45 035505	0.007554	24.200430	0.913024	-12.127131
0.542475	тэ.033373 ЛЛ 86 577 0	0.010702	22.33+334	0.91/3/3	-12.701003
いいけんグーブ	++.0UJ//U	0.024370	20.002327	0.741/44	-13.100003

0.926071	-13.409557	0.952165	-14.655924	0.978258	-15.779654
0.930422	-13.627364	0.956515	-14.850881	0.982609	-15.956434
0.934769	-13.840011	0.960862	-15.042041	0.986956	-16.130085
0.939118	-14.050266	0.965211	-15.231573	0.991304	-16.302289
0 943467	-14 255690	0.969560	-15 416999	0 995654	-16 470200
0.947816	-14 456843	0 973909	-15 599085	1 000000	-16 636229
Stop 3. INT	$2 \rightarrow TS3 \rightarrow INT3$	0.975909	15.577005	1.000000	10.03022)
Step 5: INT	$2 \rightarrow 153 \rightarrow 1013$				
		0.063538	1.076279	0.133781	3.392290
Intrinsic	Electronic	0.064863	1.109313	0.135107	3.448999
Coordinate	Energy	0.066188	1.142801	0.136433	3.506234
	(kJ/mol)	0.067513	1.176542	0.137759	3.564056
		0.068838	1.210710	0.139084	3.622439
0.000000	0.000000	0.070162	1.245141	0.140410	3.681494
0.001322	0.012164	0.071487	1.280007	0.141736	3.741127
0.002643	0.025013	0.072813	1.315228	0.143060	3.801338
0.003961	0.037847	0.074138	1.350880	0.144384	3.861538
0.005278	0.051347	0.075464	1.386926	0.145708	3.922140
0.006595	0.064810	0.076790	1.423381	0.147033	3.983319
0.007913	0.078852	0.078116	1.460253	0.148358	4.045234
0.009232	0.093334	0.079441	1.497535	0.149684	4.107805
0.010554	0.108252	0.080767	1.535303	0.151010	4.170982
0.011877	0.123766	0.082092	1.573386	0.152336	4.234745
0.013200	0.139619	0.083416	1.612060	0.153662	4.299093
0.014524	0.156096	0.084740	1.650570	0.154989	4.364030
0.015848	0.172855	0.086064	1.689669	0.156315	4.429576
0.017172	0.190262	0.087387	1.728629	0.157641	4.495767
0.018496	0.207884	0.088711	1.768303	0.158967	4.562633
0.019820	0.226145	0.090036	1.808305	0.160292	4.630169
0.021144	0.244631	0.091362	1.848885	0.161617	4.698177
0.022468	0.263695	0.092687	1.889869	0.162941	4.766522
0.023793	0.283126	0.094013	1.931323	0.164266	4.835341
0.025118	0.303067	0.095339	1.973181	0.165591	4.904886
0.026443	0.323480	0.096665	2.015483	0.166916	4.975223
0.027767	0.344324	0.097990	2.058187	0.168242	5.046321
0.029092	0.365695	0.099316	2.101343	0.169569	5.118155
0.030416	0.387432	0.100642	2.144907	0.170895	5.190713
0.031741	0.409736	0.101968	2.188945	0.172221	5.264001
0.033065	0.432354	0.103293	2.233400	0.173547	5.338027
0.034389	0.455566	0.104619	2.278349	0.174873	5.412831
0.035713	0.479064	0.105945	2.323720	0.176200	5.488408
0.037037	0.503135	0.107270	2.369606	0.177526	5.564884
0.038362	0.527515	0.108595	2.415901	0.178851	5.641989
0.039686	0.552442	0.109921	2.462706	0.180176	5.720019
0.041011	0.577747	0.111246	2.509923	0.181501	5.798246
0.042336	0.603581	0.112571	2.557639	0.182827	5.877457
0.043661	0.629831	0.113896	2.605819	0.184152	5.957396
0.044985	0.656601	0.115221	2.654509	0.185478	6.038351
0.046311	0.683783	0.116547	2.703724	0.186804	6.120198
0.047636	0.711474	0.117872	2.753464	0.188130	6.202951
0.048960	0.739538	0.119198	2.803756	0.189456	6.286589
0.050285	0.768101	0.120524	2.854570	0.190782	6.371112
0.051610	0.796994	0.121850	2.905948	0.192109	6.456530
0.052935	0.826387	0.123176	2.957846	0.193435	6.542846
0.054260	0.856120	0.124501	3.010312	0.194761	6.630068
0.055585	0.886343	0.125827	3.063284	0.196087	6.718206
0.056910	0.916935	0.127153	3.116826	0.197414	6.807268
0.058236	0.947997	0.128479	3.170850	0.198740	6.897257
0.059561	0.979430	0.129804	3.225445	0.200066	6.988186
0.060887	1.011319	0.131130	3.280515	0.201393	7.080057
0.062212	1.043571	0.132455	3,336155	0.202719	7.172877

0.204045	7.266651	0.283622	14.797250	0.363192	26.828498
0.205371	7.361380	0.284948	14.956851	0.364519	27.074048
0.206698	7.457071	0.286274	15.117682	0.365845	27.321108
0.208024	7.553729	0.287601	15.279748	0.367171	27.569669
0.209350	7 651350	0.288927	15 443075	0 368497	27 819719
0.210677	7 749940	0.290253	15 607676	0.369824	28.071253
0.210077	7.849502	0.291579	15 773563	0.307024	28.324256
0.212005	7.049302	0.201070	15.040757	0.372476	28.524230
0.213329	7.930033 9.051520	0.292900	15.940757	0.372470	20.370720
0.214033	8.031339	0.294232	16.109272	0.575805	20.001005
0.215982	8.154021	0.295558	16.279124	0.375129	29.091995
0.21/308	8.25/4/6	0.296885	16.450325	0.3/6455	29.350/8/
0.218634	8.361908	0.298211	16.622889	0.3/7/81	29.611009
0.219960	8.467319	0.299537	16.796828	0.3/9108	29.872650
0.221287	8.573715	0.300863	16.972154	0.380434	30.135707
0.222613	8.681098	0.302190	17.148876	0.381760	30.400171
0.223939	8.789470	0.303516	17.327003	0.383087	30.666040
0.225266	8.898838	0.304842	17.506550	0.384413	30.933308
0.226592	9.009212	0.306169	17.687513	0.385739	31.201972
0.227918	9.120596	0.307495	17.869914	0.387065	31.472031
0.229244	9.233001	0.308821	18.053747	0.388392	31.743476
0.230571	9.346433	0.310147	18.239049	0.389718	32.016311
0.231897	9.460908	0.311473	18.425775	0.391044	32.290531
0.233223	9.576432	0.312799	18.614013	0.392370	32.566132
0.234550	9.693018	0.314125	18.803534	0.393697	32.843115
0.235876	9.810680	0.315450	18.994526	0.395023	33.121481
0.237202	9.929423	0.316775	19.186595	0.396349	33.401228
0.238528	10.049264	0.318101	19.380147	0.397676	33.682358
0.239855	10 170210	0.319427	19 574974	0.399002	33 964878
0.241181	10 292272	0.320753	19 771359	0.400328	34 248786
0.242507	10/115/158	0.3220735	19 969183	0.100520	3/ 53/09/
0.242307	10.539776	0.322070	20 168500	0.402081	3/ 820809
0.245160	10.65235	0.324730	20.100300	0.40/207	35 108037
0.245100	10.701837	0.324750	20.507251	0.405633	35 308/08
0.240480	10.791057	0.320037	20.371441	0.405055	35.590490
0.247812	11.049495	0.327383	20.773049	0.400900	25 091066
0.249159	11.046463	0.328709	20.980076	0.408280	33.981900
0.250465	11.1/8530	0.330035	21.180517	0.409612	30.275909
0.251791	11.309738	0.331362	21.394378	0.410938	36.5/1354
0.253117	11.442089	0.332688	21.603659	0.412265	36.868324
0.254444	11.575588	0.334014	21.814366	0.413591	37.166841
0.255770	11.710231	0.335340	22.026509	0.414917	37.466927
0.257096	11.846014	0.336667	22.240099	0.416243	37.768610
0.258423	11.982932	0.337993	22.455137	0.417570	38.071916
0.259749	12.120980	0.339319	22.671641	0.418896	38.376863
0.261075	12.260153	0.340646	22.889618	0.420222	38.683474
0.262401	12.400447	0.341972	23.109079	0.421549	38.991770
0.263728	12.541859	0.343298	23.330035	0.422875	39.301769
0.265054	12.684381	0.344624	23.552499	0.424201	39.613478
0.266380	12.828012	0.345951	23.776475	0.425527	39.926911
0.267706	12.972753	0.347277	24.001980	0.426854	40.242068
0.269033	13.118600	0.348603	24.229015	0.428180	40.558950
0.270359	13.265557	0.349930	24.457588	0.429506	40.877549
0.271685	13.413622	0.351256	24.687708	0.430833	41.197857
0.273012	13.562800	0.352582	24.919377	0.432159	41.519851
0.274338	13.713097	0.353908	25,152597	0.433485	41.843512
0.275664	13.864520	0.355235	25.387372	0.434811	42,167531
0.276990	14.017077	0.356561	25.623699	0.436127	42,496674
0.278317	14,170779	0 357887	25.861577	0 443140	44 245703
0 279643	14 325631	0 359214	26 101001	0.450156	46 035370
0.280969	14 481654	0.357214	26 341967	0.457174	47 8535970
0.282296	14 638853	0 361866	26 584469	0 464192	49 695249
$\gamma \gamma \omega \omega$	1 100000.7.7	0		0.707176	1 / 11 / 14 7 7

0.471209	51.560126	0.634950	108.841255	0.660224	138.556830
0.478226	53.451426	0.635371	109.227537	0.660645	138.958783
0.485244	55.372115	0.635792	109.619590	0.661066	139.344550
0 492261	57 320840	0.636213	110 017403	0 661487	139 713325
0.492201	50 200285	0.636635	110.017405	0.661008	140.064280
0.499279	53.230285	0.030033	110.42033	0.001908	140.004289
0.506296	61.269616	0.637056	110.830413	0.662330	140.396586
0.513313	63.250151	0.63/4//	111.245730	0.662751	140.709314
0.520330	65.229626	0.637898	111.667065	0.663172	141.001545
0.527348	67.211338	0.638319	112.094541	0.663593	141.272321
0.534365	69.199970	0.638741	112.528279	0.664015	141.520691
0.541382	71.198535	0.639162	112.968339	0.664436	141.745715
0.548399	73.208652	0.639583	113.414682	0.664857	141.946510
0 555416	75 233296	0 640005	113 867160	0 665278	142 122272
0.562432	77 279447	0.640425	11/ 325518	0.665699	1/2 272287
0.560448	70 350243	0.640847	114.323310	0.666121	142.272207
0.509446	77.3372 4 3 91.400550	0.040847	114.707430	0.000121	142.393972
0.5/6464	81.490550	0.641268	115.258626	0.666542	142.492848
0.583479	83.698194	0.641689	115.732857	0.666963	142.562531
0.590492	86.015940	0.642111	116.212021	0.667384	142.604686
0.597505	88.488831	0.642532	116.696139	0.667806	142.618977
0.604516	91.176429	0.642953	117.185320	0.668227	142.605007
0.611525	94.159396	0.643374	117.679725	0.668648	142.562324
0.618525	97.570031	0.643795	118.179507	0.669069	142.490369
0.618943	97 790008	0 644217	118 684743	0 669490	142 388513
0.610364	98 01/470	0.611638	110 105376	0.660012	142.256078
0.610785	08 241274	0.044038	110.711100	0.009912	142.230078
0.019785	98.241374	0.045059	119./11190	0.070353	142.092393
0.620206	98.470748	0.045480	120.231819	0.670754	141.890851
0.620628	98.702666	0.645902	120.756795	0.6/11/5	141.668940
0.621049	98.937210	0.646323	121.285639	0.671596	141.408291
0.621470	99.174469	0.646744	121.817936	0.672018	141.114718
0.621892	99.414534	0.647166	122.353383	0.672439	140.788213
0.622313	99.657503	0.647587	122.891805	0.672860	140.428961
0.622734	99.903486	0.648008	123.433099	0.673282	140.037283
0.623155	100.152588	0.648429	123.977189	0.673703	139.613596
0.623576	100 404925	0 648850	124 523970	0 674124	139 158316
0.623998	100 660615	0 649272	125 073270	0 674545	138 671771
0.624410	100.000015	0.640603	125.673270	0.674066	130.071771
0.024419	100.919775	0.049093	125.024024	0.074900	127 (05417
0.624840	101.182525	0.650114	120.178285	0.075388	137.005417
0.625261	101.448984	0.650535	126./33221	0.6/5809	137.025436
0.625682	101.719263	0.650956	127.289123	0.676230	136.413938
0.626104	101.993479	0.651378	127.845414	0.676651	135.770667
0.626525	102.271737	0.651799	128.401472	0.677073	135.095475
0.626946	102.554138	0.652220	128.956676	0.677494	134.388391
0.627368	102.840785	0.652642	129.510451	0.677915	133.649675
0.627789	103.131767	0.653062	130.062326	0.678336	132.879818
0.628210	103.427180	0.653484	130.611917	0.678757	132.079524
0.628631	103 727107	0.653905	131 158885	0 679179	131 249667
0.629052	104 031641	0.654326	131 702857	0.679600	130 391207
0.620474	104.240967	0.654749	122 242200	0.690021	120 505140
0.029474	104.540807	0.034748	132.243300	0.080021	129.303140
0.629895	104.054880	0.055109	132.779480	0.080443	128.592414
0.630316	104.973786	0.655590	133.310474	0.680864	127.653874
0.630737	105.297707	0.656011	133.835251	0.681285	126.690231
0.631159	105.626774	0.656432	134.352800	0.681706	125.702064
0.631580	105.961139	0.656854	134.862226	0.682127	124.689852
0.632001	106.300955	0.657275	135.362762	0.682549	123.654056
0.632422	106.646376	0.657696	135.853738	0.682970	122.595184
0.632843	106.997529	0.658117	136.334493	0.683391	121,513869
0.633265	107.354511	0.658538	136.804300	0.683812	120.410925
0.633686	107 717373	0.658960	137 262340	0.684233	110 287361
0.63/107	107.717575	0.050500	137.202340	0.004233	118 1//240
0.034107	100.000133	0.037301	129 120522	0.004033	116.092042
0.034329	100.400770	0.039802	130.137322	0.0000/0	110.903243

0.685497	115.805410	0.710771	52.653008	0.736045	24.845395
0.685919	114.612283	0.711192	51.962767	0.736466	24.560539
0.686340	113.405267	0.711614	51.282889	0.736888	24.280044
0.686761	112,185696	0.712035	50.613192	0.737309	24.003854
0.687182	110 954838	0.712456	49 953451	0 737730	23 731905
0.687603	109 713895	0.712130	19.993191	0.738151	23.751703
0.688025	109.715095	0.712077	48 662842	0.738572	23.404145
0.688446	107 206367	0.713220	48.002042	0.738004	22.040044
0.000440	107.200507	0.713720	40.051400	0.730994	22.940944
0.000007	103.942104	0.714141 0.714562	47.409137	0.739413	22.003394
0.089288	104.072405	0.714562	40./9500/	0.739830	22.455805
0.689709	103.398743	0.714983	46.190744	0.740257	22.186123
0.690131	102.122299	0.715405	45.594420	0.740679	21.942293
0.690552	100.844549	0.715826	45.006536	0.741100	21.702260
0.690973	99.566934	0.716247	44.42/00/	0.741521	21.465970
0.691394	98.290893	0.716668	43.855753	0.741942	21.233369
0.691816	97.017851	0.717089	43.292702	0.742363	21.004402
0.692237	95.749173	0.717511	42.737760	0.742785	20.779021
0.692658	94.486158	0.717932	42.190832	0.743206	20.557169
0.693080	93.230014	0.718353	41.651796	0.743627	20.338793
0.693501	91.981851	0.718775	41.120521	0.744049	20.123846
0.693922	90.742683	0.719196	40.596870	0.744470	19.912270
0.694343	89.513445	0.719617	40.080697	0.744891	19.704020
0.694764	88.295035	0.720038	39.571869	0.745312	19.499048
0.695186	87.088336	0.720459	39.070260	0.745733	19.297302
0.695607	85.894230	0.720881	38.575755	0.746155	19.098735
0.696028	84.713590	0.721302	38.088260	0.746576	18.903303
0.696449	83.547204	0.721723	37.607680	0.746997	18.710962
0.696870	82 395715	0 722144	37 133940	0 747418	18 521669
0.697292	81 259566	0.722565	36 666956	0 747839	18 335379
0.697713	80 138982	0.722987	36 206653	0.748261	18 152053
0.608134	70.034032	0.722/08	35 752956	0.748682	17 071653
0.098134	77.034032	0.723408	35.752950	0.740002	17.704140
0.098550	76 971090	0.723029	24 865050	0.749105	17.794140
0.098977	70.071000	0.724231	34.803039	0.749323	17.019476
0.099398	73.013242	0.724072	34.430702	0.749940	17.447029
0.099819	74.771404	0.725095	34.002038	0.750307	17.112242
0.700240	/3./45/90	0.725514	33.580788	0.750788	17.112242
0.700662	72.736519	0.725935	33.1650/4	0.751209	16.948634
0.701083	/1./43544	0.726357	32.755418	0.751631	16./8//12
0.701504	70.766598	0.726778	32.351747	0.752052	16.629442
0.701925	69.805221	0.727199	31.953981	0.752473	16.473792
0.702346	68.858831	0.727620	31.562049	0.752894	16.320735
0.702768	67.926836	0.728042	31.175878	0.753316	16.170244
0.703189	67.008736	0.728463	30.795395	0.753737	16.022290
0.703610	66.104180	0.728884	30.420534	0.754158	15.876842
0.704031	65.212993	0.729305	30.051229	0.754580	15.733878
0.704452	64.335131	0.729726	29.687413	0.755000	15.593370
0.704874	63.470612	0.730148	29.329030	0.755422	15.455289
0.705295	62.619440	0.730569	28.976013	0.755843	15.319611
0.705716	61.781546	0.730990	28.628300	0.756264	15.186312
0.706138	60.956748	0.731412	28.285832	0.756686	15.055365
0.706559	60.144741	0.731833	27.948539	0.757107	14.926745
0.706980	59.345137	0.732254	27.616361	0.757528	14.800427
0 707401	58 557511	0 732675	27 289226	0 757949	14 676390
0 707822	57 781445	0.733096	26 967070	0 758370	14 554604
0 708244	57 016570	0.7335070	26.507070	0.758707	14 /350/0
0.708665	56 7676/2	0.733030	20.049017	0.750792	1/ 317700
0.700000	55 510/61	0.73737	20.337377	0.757215	14 202525
0.709080	JJ.J17401 54 706020	0.734300	20.029/40	0./39034	14.202333
0.709307	J4./00939 54.065020	0.725202	25.120189	0./00000	14.089323
0.709928	54.005059	0.755202	23.428430	0./004/0	13.9/8030
0./10350	22.222/39	0.755624	23.134681	U. / 6U898	1.3.809889

0.761319	13.763212	0.827303	9.131796	0.879407	8.254076
0.761740	13.658602	0.828171	9.115122	0.880275	8.240906
0.762162	13.556031	0.829040	9.098555	0.881144	8.227776
0.762583	13.455480	0.829908	9.082098	0.882012	8.214683
0.763004	13.356921	0.830777	9.065744	0.882881	8.201624
0.763425	13.260335	0.831645	9.049487	0.883750	8.188601
0.763847	13.165696	0.832514	9.033324	0.884618	8.175613
0.764268	13.072981	0.833382	9.017256	0.885486	8.162658
0 764689	12.982168	0.834251	9 001275	0.886354	8 149744
0.765110	12.893232	0.835119	8 985380	0.887222	8 136876
0.765531	12.806152	0.835988	8 969567	0.888090	8 124066
0.765953	12.000132	0.836856	8 953832	0.888957	8 111312
0.765374	12.720905	0.830850	8 038170	0.880824	8.008500
0.766705	12.037400	0.838504	8 022500	0.800601	8.090377
0.767217	12.333011	0.830462	8.007003	0.890091	8.003044
0.767627	12.473717	0.839402	8.907093 9.901657	0.091336	8.073003
0.767057	12.397703	0.840330	0.091037	0.092420	8.000239
0.768059	12.321324	0.841199	8.8/0290	0.893294	8.04/499
0.768480	12.240574	0.842068	8.860994	0.894162	8.034776
0.768901	12.173490	0.842936	8.845/64	0.895030	8.022094
0.769323	12.102051	0.843805	8.830596	0.895899	8.009442
0.769744	12.032220	0.844673	8.815494	0.896767	7.996819
0.776355	11.12/688	0.845542	8.800453	0.89/636	7.984219
0.782952	10.534792	0.846410	8.785474	0.898505	7.971643
0.789513	10.148847	0.847279	8.770556	0.899373	7.959088
0.796078	9.886417	0.848147	8.755696	0.900242	7.946554
0.796905	9.855930	0.849016	8.740893	0.901110	7.934038
0.797774	9.828446	0.849885	8.726146	0.901978	7.921546
0.798642	9.801204	0.850753	8.711456	0.902847	7.909069
0.799510	9.774779	0.851621	8.696822	0.903716	7.896614
0.800379	9.749072	0.852490	8.682242	0.904584	7.884177
0.801247	9.724009	0.853358	8.667718	0.905453	7.871756
0.802116	9.699526	0.854227	8.653246	0.906321	7.859355
0.802984	9.675574	0.855096	8.638827	0.907190	7.846971
0.803853	9.652113	0.855964	8.624460	0.908058	7.834605
0.804721	9.629105	0.856833	8.610146	0.908927	7.822255
0.805590	9.606523	0.857701	8.595882	0.909795	7.809923
0.806458	9.584340	0.858570	8.581667	0.910664	7.797609
0.807327	9.562536	0.859438	8.567500	0.911533	7.785311
0.808195	9.541088	0.860307	8.553383	0.912401	7.773034
0.809064	9.519979	0.861175	8.539310	0.913269	7.760778
0.809932	9.499193	0.862044	8.525287	0.914137	7.748546
0.810801	9.478714	0.862912	8.511309	0.915006	7.736340
0.811669	9.458527	0.863781	8.497378	0.915874	7.724179
0.812538	9 438615	0 864649	8 483489	0 916741	7 712041
0.813406	9 418968	0.865518	8 469650	0.917608	7 699977
0.814275	9 399574	0.866387	8 455853	0.918475	7 687847
0.815144	9 380/15	0.867255	8 442101	0.9104/3	7.675775
0.816012	0 361/88	0.868124	8 128303	0.919342	7.663580
0.816880	9342776	0.868992	8 /1/730	0.921077	7.651466
0.817740	0 32/260	0.860861	8 /01100	0.921077	7.630315
0.017749	9.524209	0.809801	0.401109	0.921945	7.039313
0.010017	9.303901	0.870729	0.307333	0.922014	7.027250
0.019400	7.20/030	0.0/1398	0.374000	0.923082	7 602100
0.020333	7.207072	0.0/2400	0.300332	0.924330	7.003122
0.821223	9.232113	0.0/3333	0.34/142	0.923418	7.391100
0.822092	9.234300	0.874201	8.333828 8.220 <i>C</i> 45	0.926287	7.579120
0.822960	9.21/038	0.8/506/	ð.320043 9.207271	0.92/155	1.56/153
0.823828	9.199723	0.8/5935	8.30/2/1	0.928024	1.555215
0.824697	9.182547	0.876802	8.293947	0.928892	1.543298
0.825566	9.165505	0.877670	8.280567	0.929761	7.531410
0.826434	9.148592	0.878538	8.267298	0.930629	7.519545

0.931498	7.507709	0.954915	7.200925	0.978315	6.923268
0.932366	7.495897	0.955782	7.190008	0.979181	6.913687
0.933234	7.484122	0.956650	7.179067	0.980049	6.904031
0.934102	7.472373	0.957517	7.168282	0.980916	6.894524
0.934971	7.460671	0.958385	7.157575	0.981783	6.884985
0.935839	7.448998	0.959252	7.147023	0.982651	6.875570
0.936706	7.437409	0.960118	7.136679	0.983518	6.866158
0.937573	7.425833	0.960983	7.126295	0.984386	6.856866
0.938440	7.414378	0.961849	7.116063	0.985253	6.847588
0.939306	7.402849	0.962715	7.105225	0.986121	6.838438
0.940172	7.391365	0.963582	7.094563	0.986987	6.829293
0.941039	7.379803	0.964450	7.083864	0.987854	6.820248
0.941906	7.368258	0.965318	7.073346	0.988721	6.811182
0.942774	7.356769	0.966186	7.062921	0.989588	6.802151
0.943642	7.345314	0.967054	7.052581	0.990455	6.793145
0.944509	7.333940	0.967922	7.042316	0.991322	6.784171
0.945377	7.322588	0.968790	7.032129	0.992190	6.775281
0.946245	7.311316	0.969657	7.022044	0.993058	6.766433
0.947113	7.300056	0.970523	7.012130	0.993925	6.757680
0.947980	7.288892	0.971387	7.002300	0.994793	6.748971
0.948848	7.277736	0.972251	6.992657	0.995661	6.740349
0.949715	7.266696	0.973116	6.982473	0.996529	6.731764
0.950582	7.255682	0.973981	6.972616	0.997397	6.723260
0.951449	7.244750	0.974848	6.962427	0.998264	6.714777
0.952315	7.233901	0.975714	6.952636	0.999132	6.706372
0.953181	7.222900	0.976581	6.942712	1.000000	6.698002
0.954048	7.212028	0.977448	6.933040		

Step 4: INT3 \rightarrow TS4 \rightarrow P + H₂O

		0.033353	1.635385	0.073380	5.017987
Intrinsic	Electronic	0.034684	1.720214	0.074716	5.171237
Coordinate	Energy	0.036011	1.804228	0.076051	5.327801
	(kJ/mol)	0.037338	1.888706	0.077385	5.487744
		0.038668	1.975852	0.078721	5.651134
0.000000	0.000000	0.040001	2.065518	0.080056	5.818029
0.001334	0.050916	0.041336	2.157216	0.081392	5.988492
0.002668	0.102980	0.042671	2.250789	0.082726	6.162584
0.004004	0.156102	0.044007	2.346220	0.084061	6.340354
0.005339	0.210305	0.045341	2.443537	0.085397	6.521860
0.006675	0.265606	0.046677	2.542781	0.086732	6.707147
0.008010	0.322028	0.048012	2.643994	0.088068	6.896262
0.009344	0.379597	0.049347	2.747226	0.089402	7.089246
0.010680	0.438325	0.050683	2.852530	0.090737	7.286146
0.012015	0.498249	0.052017	2.959955	0.092073	7.486997
0.013351	0.559379	0.053352	3.069559	0.093408	7.691828
0.014685	0.621779	0.054688	3.181400	0.094742	7.900673
0.016020	0.685468	0.056023	3.295535	0.096078	8.113562
0.017355	0.750720	0.057359	3.412029	0.097413	8.330512
0.018687	0.817134	0.058693	3.530946	0.098749	8.551548
0.020020	0.885216	0.060028	3.652346	0.100084	8.776687
0.021349	0.952925	0.061364	3.776299	0.101418	9.005938
0.022679	1.022367	0.062699	3.902871	0.102754	9.239316
0.024011	1.093221	0.064035	4.032130	0.104089	9.476824
0.025345	1.165916	0.065369	4.164145	0.105425	9.718467
0.026680	1.240142	0.066704	4.298986	0.106760	9.964250
0.028014	1.315895	0.068040	4.436720	0.108095	10.214166
0.029350	1.393145	0.069375	4.577415	0.109430	10.468212
0.030685	1.471971	0.070709	4.721145	0.110765	10.726380
0.032020	1.552571	0.072045	4.867979	0.112101	10.988665

0.113436	11.255049	0.193548	33.464166	0.273659	61.858242
0.114771	11.525520	0.194883	33.910806	0.274994	62.339334
0.116106	11.800063	0.196217	34.359044	0.276330	62.820142
0.117441	12.078657	0.197553	34.808845	0.277664	63.300645
0.118777	12.361282	0.198888	35.260166	0.279000	63,780820
0.120111	12.647916	0.200224	35 712973	0.280335	64 260635
0.121447	12.047710	0.200224	36 167226	0.280555	64 740073
0.121447	12.930332	0.201333	36 622887	0.281070	65 210100
0.122762	12.233100	0.202893	30.022007	0.283000	65 607602
0.124117	13.331012	0.204229	37.079918	0.284540	03.09/092
0.125455	13.834019	0.205564	37.338283	0.2850/0	00.1/5819
0.126/8/	14.140292	0.206900	37.997945	0.28/011	66.653458
0.128123	14.450403	0.208234	38.458862	0.288346	67.130577
0.129458	14.764318	0.209569	38.921005	0.289682	67.607153
0.130/93	15.082001	0.210905	39.384333	0.291016	68.083153
0.132129	15.403415	0.212240	39.848807	0.292352	68.558553
0.133463	15.728522	0.213576	40.314395	0.293687	69.033327
0.134799	16.057285	0.214910	40.781059	0.295022	69.507450
0.136134	16.389663	0.216246	41.248766	0.296357	69.980896
0.137469	16.725619	0.217581	41.717473	0.297692	70.453641
0.138805	17.065107	0.218916	42.187151	0.299028	70.925664
0.140139	17.408089	0.220252	42.657759	0.300363	71.396939
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0.905201 -44.671457

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